

Cruise Report for P8S

A hydrographic Section along 130°E

20 December 1996

R/V KAIYO

17 Jun. 1996 - 2 Jul. 1996

Cruise report of WOCE P8S

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A. Cruise narrative

A.1 Highlights

A.1.a WOCE designation : P8S

A.1.b EXPOCODE : 49XK9605

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A.1.d Ship : R/V Kaiyo

A.1.e Ports of call : Yokosuka, Japan-Korol, Palau

A.1.f Cruise dates : June 17,1996-July 2, 1996

A.2 Cruise Summary Information

A.2.a Geographic boundaries

A.2.b Stations occupied

The 27 CTD stations are located between 10-00N, 130-00E to 00-45N, 130-00E, and distance between two stations are minimum of 15 miles near the Indonesian coast and maximum of 30 miles on the open ocean with smooth bottom topography.

Standard sampling layers are designed as 10, 20, 30, 50, 75, 100, 125, 150, 200, 250, 300, 400, 500, 600, 700, 800, 900, 1000 m and below that level,

sampling layers are designed as 250 m interval to the just above the bottom. One casting operation of the Rosette sampler with 36 bottles can satisfy the standard sampling at the area shallower than water depth of 5250 m. At the station deeper than this critical water depth, samplings at the depth of 20, 75 and 125 m were occasionally omitted. At the assistant CTD station on 02-45N, we made CTD observation at layers shallower than 1000 m.

Sampling elements are as follows: Salinity, Dissolved Oxygen, Nutrients (Nitrate, Nitrite, Phosphate and Silicate) were measured at all layers on all stations except the assistant station. Alkalinity, pH and TCO₂ were measured at all layers on some stations, and H-3, He-3 and C-14 were sampled at some layers on these stations with a little of exceptions.

A.2.c Floats and drifters deployed

A.2.d Moorings deployed or recovered

A.3 List of Principal Investigators

Table A.3-1 : List of parameters to be measured and principal investigators

Parameter/Instr.	Affiliation	Principal Investigator
CTD/Rosette	JAMSTEC	Yuji Kashino (CTD Software)
	JAMSTEC	Hiroyuki Yoritaka(Hardware)
ADCP	JAMSTEC	Yuji Kashino
Salinity	JAMSTEC	Hiroyuki Yoritaka
NO ₃ ,NO ₂ ,PO ₄ ,SiO ₂	JAMSTEC	Chizuru Saito
DO	NME	Misumi Aoki
C-14,H-3,He-3	JAMSTEC	Chizuru Saito
TCO ₂ ,pH,Alkalinity	CRIEPI	Kiminori Shitashima

JAMSTEC : Japan Marine Science and Technology Center, Japan

NME : Nippon Marine Enterprise, c/o, Ltd., Japan

CRIEPI : Central Research Institute Electric Power Industry, Japan

A.4 Scientific Program and Methods

The principal objectives of the cruise were:

To submit a data set to the WHPO, and contribute the global measurement of the WOCE program.

To investigate southward intrusion of low salinity water (<34.5 pss-78), which may be advected from the North Pacific ocean to a layer below the high salinity Tropical Pacific water. CTD point at 02-45N, 130-00E was added for this sake.

A.5 Major Problems and Goals not Achieved

At Stn.12 (05-30N,130-00E) on June 26, we encountered a trouble with damage on a fiber of armored-wire of the CTD cable. After this accident, irregular winding of the CTD cable over 5000 m long on the winch wheel was occurred. But there was no influence on the CTD signal, we could carried out all of the originally planned CTD observations on schedule.

A.6 Other Incidents of Note

A.7 List of Cruise Participants

Table A.7-2. Cruise Participants

Name	Affiliation	Parameter
Noriya Yoshioka	JAMSTEC	CTD
Hiroyuki Yoritaka	JAMSTEC	Salinity / CTD Hardware
Yuji Kashino	JAMSTEC	CTD Software /ADCP
Hirofumi Yamamoto	JAMSTEC	CTD
Chizuru Saito	JAMSTEC	Nutrients / C-14 / H-3 / He-3
Naomi Harada	JAMSTEC	C-14 / H-3 / He-3
Misumi Aoki	NME	DO
Hiroshi Yamamoto	NME	CTD
Atsuo Ito	NME	Salinity
Mitsuru Hayashi	NME	Salinity
Masayuki Fujisaki	NME	DO

Nobuharu Komai	NME	Nutrients
Takeshi Katayama	NME	CTD
Satoru Kanda	NME	CTD
Takehiko Shiribiki	STM	DO
Yasuko Nogiwa	KEEC	Nutrients
Kiyotaka Nakao	KEEC	Nutrients
Kiminori Shitashima	CRIEPI	TCO2 / pH / Alkalinity
Daisuke Tsumune	CRIEPI	TCO2 / pH / Alkalinity
Steven B. Kraines	CRIEPI	TCO2 / pH / Alkalinity
Djoko Hartoyo	BPPT	CTD
R. Trimanadi	BPPT	CTD
Victoriano C. Buquir	c/o NAMRIA (Philippine)	CTD

JAMSTEC : Japan Marine Science and Technology Center, Japan

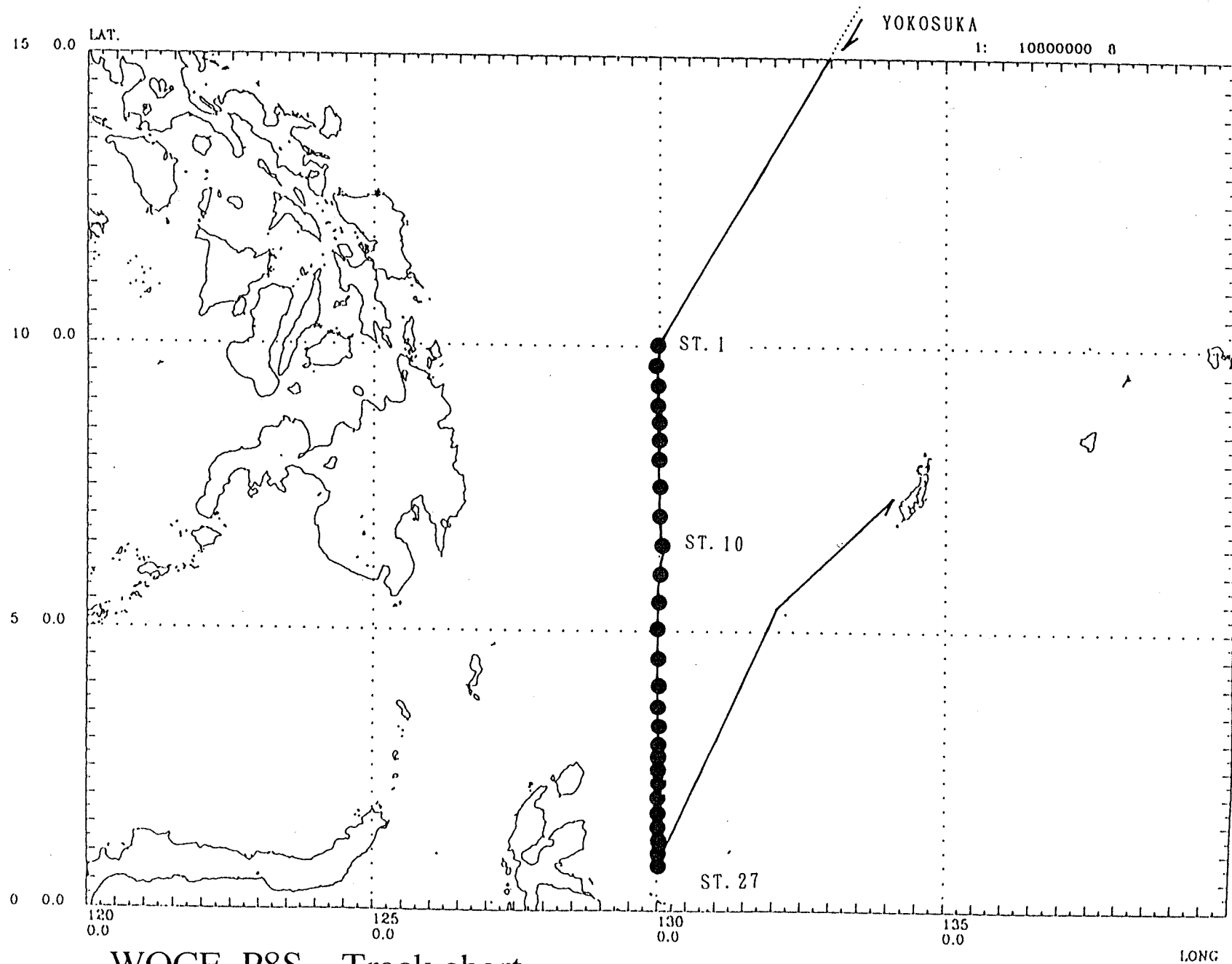
NME : Nippon Marine Enterprises, c/o Ltd., Japan

STM : Sanyo Techno Marine, Inc., Japan

KEEC : Kansai Environmental Engineering Center, c/o Ltd., Japan

CRIEPI : Central Research Institute of Electric Power Industry, Japan

BPPT : Badan Pengkajian dan Penerapan Teknologi, Indonesia



WOCE P8S Track chart

B. Underway Measurement

B.1 Navigation and bathymetry (Echosounding)

by Y.Kashino (19 November 1996)

The water depth obtained by the multi-narrow beam echo-sounder (General Instrument) and corrected depth are summarized in Table B.1-1. The corrected depth are derived from CTD depth plus altimeter value. This result shows tendency of decrease of its difference. After Stn.18, the depth measured from echosounding is larger than corrected depth.

Except at few stations, the differences are less than $\pm 1.0\%$.

Table B.1-1. The differences between corrected water depth and uncorrected echosounding depth. The values of the corrected depths are derived from CTD depth plus altimeter value.

Station number	Corrected depth (meter)	echosounding (uncorrected) (meter)	Diff. (meter)
01	5939	5913	26
02	5751	5761	-10
03	6005	5942	63
04	5924	5865	59
05	5963	5978	-15
06	6002	5827	175
07	5662	5612	50
08	5537	5520	17
09	5549	5520	29
10	5549	5526	23
11	5488	5476	12
12	5466	5450	16
13	5039	5038	1
14	4856	4845	11
15	4693	4709	-16
16	3703	3615	88
17	3885	3886	-1
18	3005	3016	-11
19	-----	3032	-----
20	4000	4023	-23
21	4308	4317	-9
22	4394	4396	-2
23	3862	3890	-28
24	4121	4113	8
25	-----	3299	-----
26	3003	3022	-19
27	1451	1514	-53

B.2 Acoustic Doppler Current Profiler (ADCP)

by Y.Kashino (2 September 1996)

a. System

The RD narrow band Acoustic Doppler Current Profiler (ADCP) by RD Instruments was used to observe current structure along the cruise track from Yokosuka to Palau including south of P8 line. This ADCP transmits 75KHz acoustic pluses from the transducer along 4 beams angled of 30 degree.

The ADCP was controlled by the software "TRANSECT" developed by RD Instruments on IBM PS/V model 2408.

b. Data processing

Raw data was acquired every a minute at 51 layers from 30m to 830m every 16m. We report averaged data every 10 km for all layers. Data processing was done as follows:

- 1) Convert binary data to ASCII processed data outputted every one minute using TRANSECT.

- 2) Remove noise from processed data. The noise is defined as follows:

- Data during the period of ship velocity of < 5 knot with 10 minutes before and after.
- Data with vertical averaged velocity (from 30m depth to the depth where data is available) of > 1.0 m/s, which is probably derived from GPS error.
- Data with percent good of < 50 .
- Data with its difference from 24 samples average of > 3 sigma.

- 3) Calculate average velocity every 10 km segment.

The format of averaged data is shown in Table B.2-1. Unit of velocity is (m/sec).

We did not correct the gyrocompass error because it was less than 0.2 degree when we check it in Palau. We did not also correct the error from beam angle setting error because we could not find systematic error when we checked the data obtained during the cruise conducted in January, 1996.

c. Primary result

The meridional and zonal velocity section plot along P8 line and vector plot at

50m and 350m level are shown in Fig. F.1-10, F.1-11, F.2-1 and F.2-7 using averaged data. We can see anticyclonic Halmahera eddy clearly. We can also see the low salinity water from the North Pacific advected by southward flow below the South Pacific Tropical Water comparing meridional velocity section and salinity section along P8 line.

Table B.2-1 Format of averaged data in 10km segments.

Line	Field	Description
------	-------	-------------

Following five lines are header of this file.

- | | | |
|---|---|--|
| A | 1 | Expocode and cruise date |
| B | 1 | Place where observation was started and ended |
| C | 1 | Length of the segment for averaging and the number of segments |
| D | 1 | Number, range, and thickness of layer |
| E | 1 | Separator |

Following are written each 10 km segments. -9.0 is assigned for "bad data" or "no data". The first five lines contain the information of segment (e.g., number of segment, location of center of segments). Starting line 6, information in columns based on the bin depth is written.

- | | | |
|---|---|--|
| 1 | 1 | Serial number of segment. |
| | 2 | Number of samples used for averaging location. |
| 2 | 1 | Mean time (UT) - Month |
| | 2 | - Day |
| | 3 | - Year |
| | 4 | - Hour |
| | 5 | - Minute |
| 3 | 1 | Location - Latitude |
| | 2 | - Longitude |
| 4 | 1 | Name of fields written below line 6 |
| 5 | 1 | Unit of fields written below line 6 |
| 6 | 1 | Depth (m) |
| | 2 | Velocity magnitude (m/sec) |

- | 3 | Velocity direction (degree)
 - | 4 | East velocity component (m/sec) - east(+)/west(-)
 - | 5 | North velocity component (m/sec) - north(+)/south(-)
 - | 6 | Number of samples used for averaging value in this layer
-

B.3 Thermosalinograph and underway dissolved oxygen, fluorometer, etc.

B.4 XBT and XCTD

B.5 Meteorological observations

by S.Ishida(Captain of R/V KAIYO) and N.Yoshioka (September 1996)

Routine weather observation with 24 hours intervals are carried out on our cruise. Aneroid barometer(Yanagi INSTRUMENT,TYPE 8A,S/N 6869) at the 13.7 m height from sea surface was used. Wind vane and anemometer(Ogasawara keiki,PR350) is at the height of 27.2 m and wind force is estimated by handy calcurater. Sea water pumped up from the depth of 4.8 m is measured its temperature, and air temperature was measured with a ventilated psychrometer(Ohta keiki,S/N 221705). These instruments were not calibrated except the barometer which was calibrated on July.4,1994.

YYMMDD/HH (UST)	DEG MIN(N)	DEG MIN(E)	DIR	FOR	WEA.	BAR.	AR.T	SST
960623/03	10.06 N	130.03 E	ENE	1	C	1008.6	25.5	29.0
960624/03	08.59 N	129.59 E	CLM	-	BC	1009.8	32.4	29.0
960625/03	07.30 N	130.00 E	SSW	2	BC	1009.3	29.8	29.0
960626/03	06.00 N	130.00 E	NW	2	BC	1012.8	31.8	29.0
960627/03	04.10 N	130.00 E	SSE	2	BC	1010.6	31.2	29.0
960628/03	02.45 N	130.00 E	SE	4	R	1013.8	26.0	29.0
960629/03	01.56 N	130.00 E	ESE	2	BC	1010.5	31.1	28.0
960630/03	01.00 N	130.00 E	NE	4	Q	1011.2	28.0	28.0
960701/03	03.42 N	131.17 E	E	1	C	1011.0	30.5	28.0

B.6 Atmospheric chemistry

C. Hydrographic Measurements - Descriptions, Techniques and Calibrations

C.1 Sampling/measurements equipments

by H. Yoritaka (September 1996)

Small-Volume Sampling : 36-place rosettes with 12-liter bottles.

CTD System : SBE-911plus CTD System with altimeter and O₂ sensor.

Winch and Cable : Tsurumi Seiki TS-10PVCTD winches having 8000 meters cable of 10.6 mm diameter. The maximum rolling load is 3800 kg x 47 m/minute.

ADCP : shipboard RD narrow band ADCP at 75 kHz.

Salinometer : Guildline Autosal 8400B with HP 2804A quartz thermometer.

Oxygen Analysis : Carpenter method. Automated potentiometric and photometric titration. Two lags of Metrohm 716 DMS Titrino.

Nutrient Analysis : Bran Luebbe Traacs 800 4 channels systems.

TCO₂ : UIC Carbon coulometer System 140

pH : RC PHM93 reference pH meter

Alkalinity : RC VIT90 Video Titrator, ABU91 Autoburette and SAM90 Sample Station

C.2 CTD/Rosette hardware

by H. Yoritaka, Y. Kashino, H. Yamamoto, M. Hayashi, K. katayama and S. Kanda (September 1996)

1. Instruments

SBE9plus CTD for 10,500 meters with the 12-liters 36-positions intelligent GO rosette water sampler (GO1016) was used during the cruise. CTD system was constructed with following sensors ;

Sensor	Model	Primary	Secondary
Temperature	SBE3	S/N 1462	S/N 1465
Conductivity	SBE4	S/N 1045	S/N 11742
Oxygen	SBE13	S/N 0311	
Pressure	Digiquarts	S/N 41223	
Pump	SBE5	S/N 0846	S/N 0847
Altimeter	Bentos 2110-1	DATASONIC	PSA-900A

Temperature and Conductivity sensors were rinsed with fresh water and pure water after each casts, and were rinsed with Triton-X detergent after each two casts.

In each thermometer frames attached on the Niskin bottles for odd number (18 bottles), two SIS digital reversing thermometers and SIS digital reversing pressure meter was fitted. The wire was a single conductor 10.6 mm armored cable manufactured by Rochester Corporation, and the winch was built by Tsurumi Seiki Japan.

2. CTD Sensors Performance

The differences between primary and secondary sensors for temperature and conductivity are shown in Fig.C.2-1. These values are performed with average of differences for 500 db - bottom in raw data at down cast. The differences are within 0.0005 deg.C in temperature. In conductivity, differences are within 0.001 - 0.0015 S/m except for initial drift.

The change of the deck pressure is shown in Fig.C.2-2. While the deck pressure at pre-cast varies within -0.6 - -0.3, it varies within +0.2 - +0.5 at post-cast except for the shallow casts (St.19: 1000db, St. 27: 1500db). The deck pressure had a hysteresis within 0.6 - 1.0 db at the deep casts.

3. CTD Sensor Calibration

The calibrations of the temperature and conductivity sensors were

conducted by Northwest Regional Calibration Center, USA on April 1996 (pre-cruise calibration) and on August 1996 (post-cruise calibration). The drift of temperature relative to the pre-cruise calibration during these 4 months was reported to be -1.01 mdeg.C for the primary temperature sensor. This tendency was consistent with previous calibrations. According to this result, the drift for the primary temperature sensor during the cruise was estimated to be -0.5 mdeg.C.

The calibration of the pressure sensor was carried out by ourselves on June 1996 (pre-cruise calibration) and on October 1996 (post-cruise calibration) with dead-weight tester manufactured by Bundenberg Co. Ltd.. Fig.C.2-3 shows difference in pressure between dead-weight tester and CTD calculated with initial coefficients at the factory. Difference between pre-cruise and post-cruise calibration was less than 0.37 db. And hysteresis in each pressure was less than 0.14 db. So the linear coefficient 0.99900 derived from the post-cruise calibration was adopted for correction.

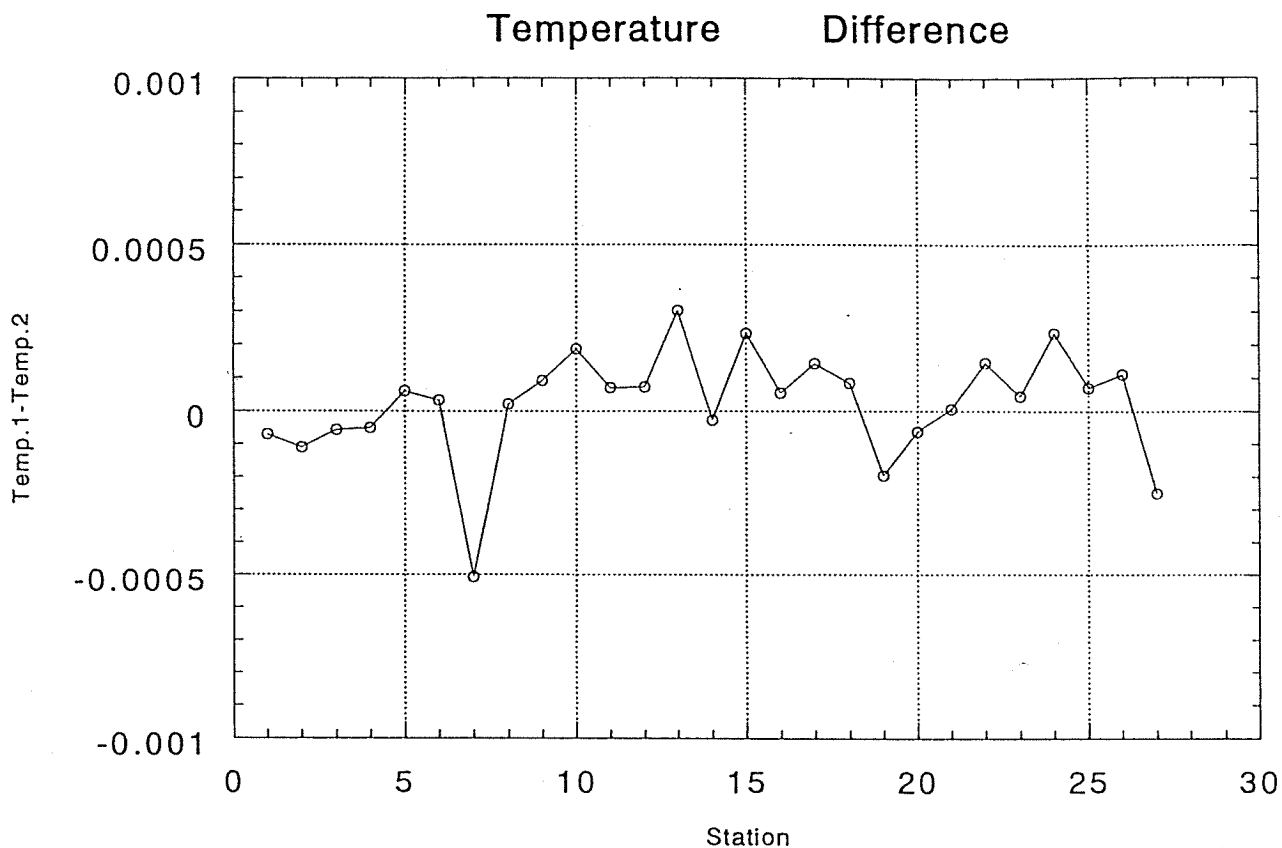


Fig. C.2-1a Differences between primary and secondary sensors in temperature.

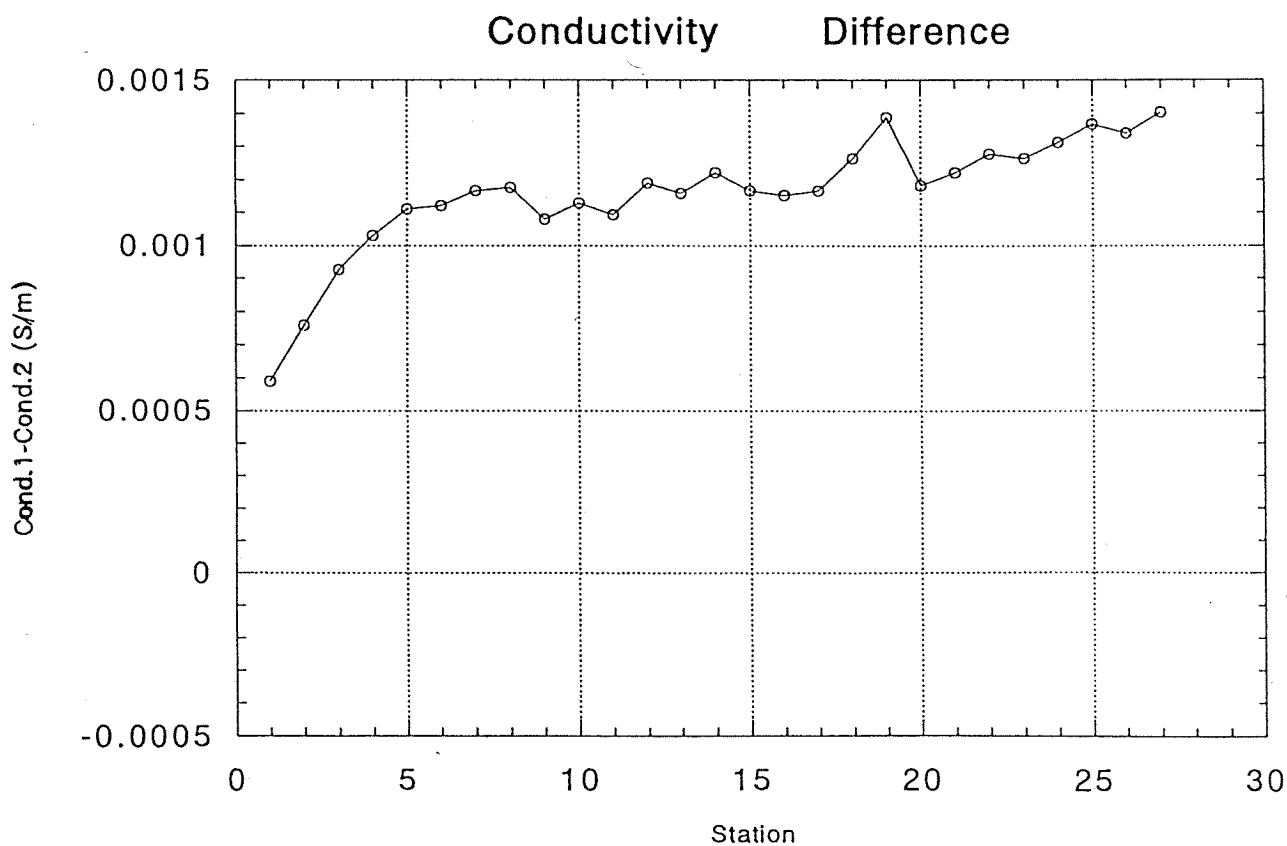


Fig. C.2-1b Differences between primary and secondary sensors in conductivity.

CTD Pressure on Deck

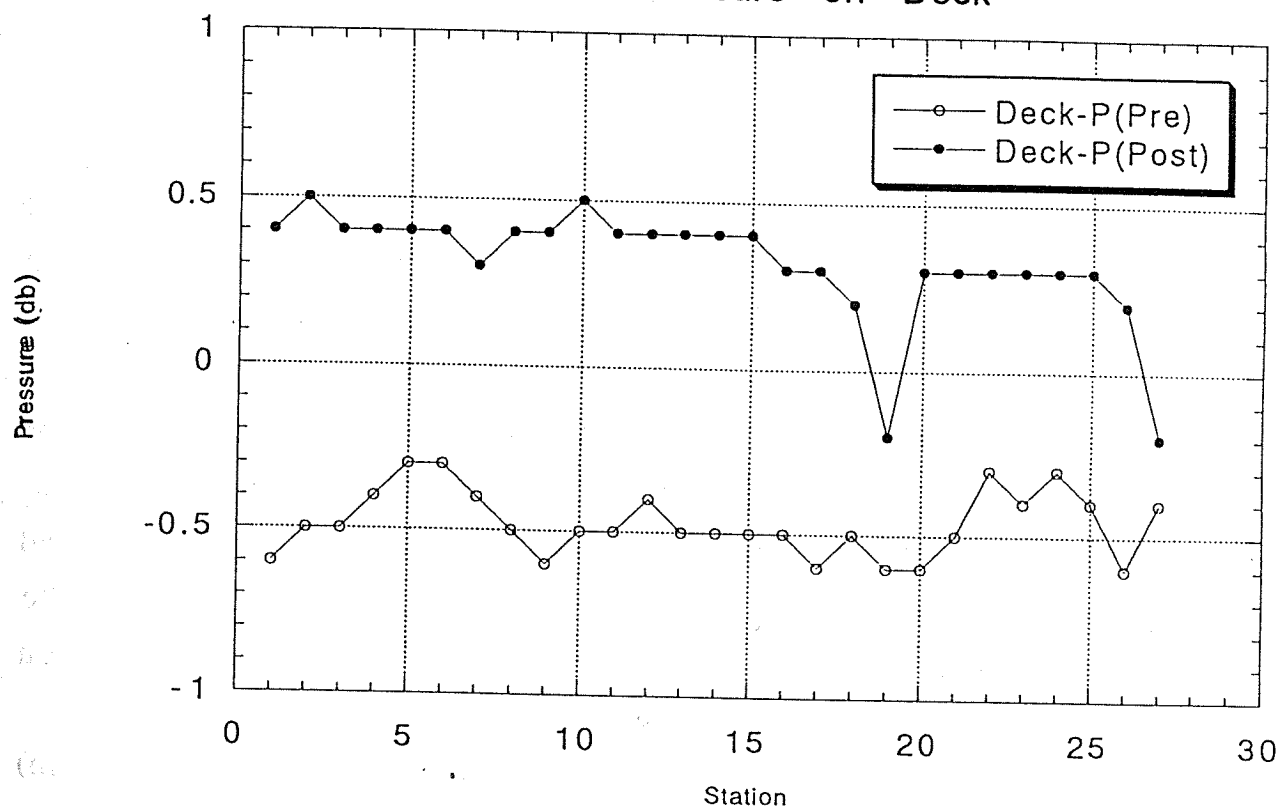


Fig. C.2-2 CTD pressure on deck at pre-cast (open circle) and post-cast (closed circle).

Difference in Pressure

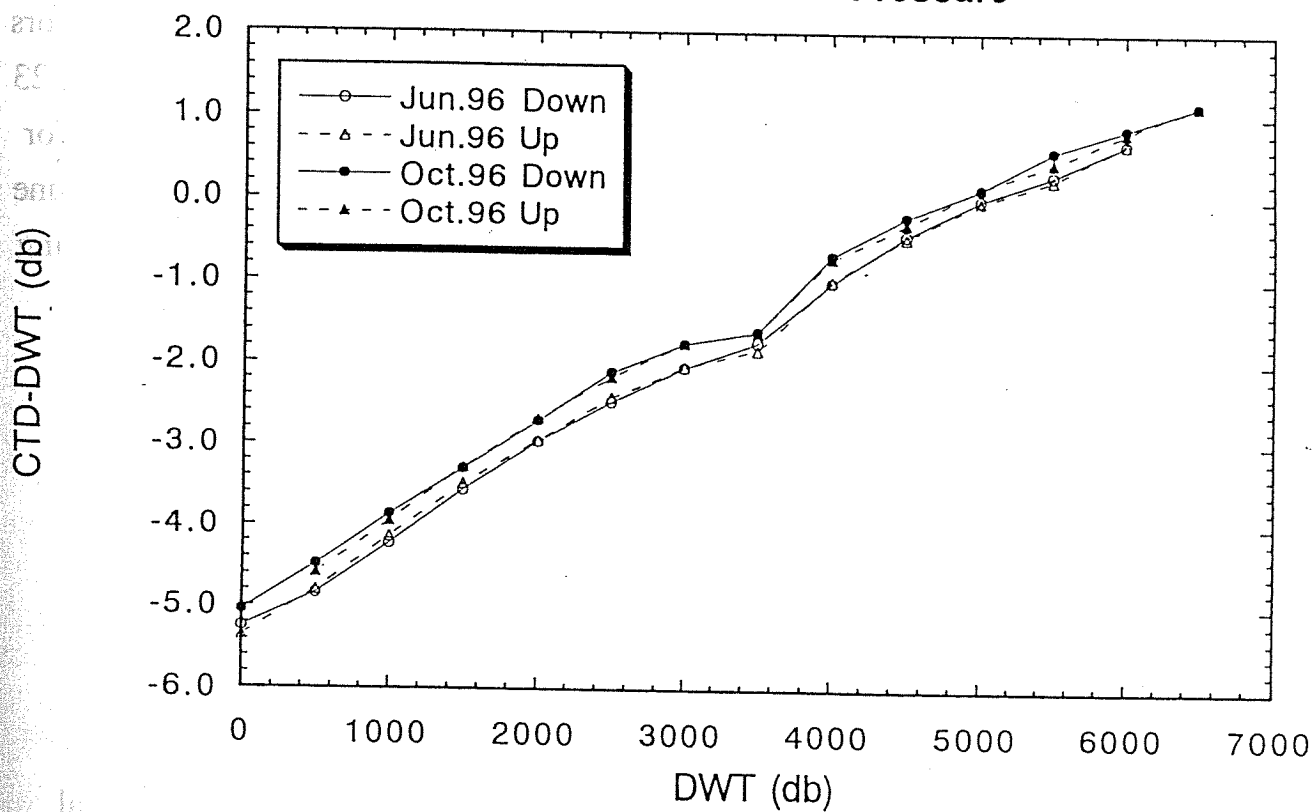


Fig. C.2-3 Laboratory calibration in pressure, at pre-cruise and post-cruise.

C.3 CTD data processing

by Y. Kashino (2 September 1996)

Introduction

The CTD data was acquired by SBE 911 plus system with frequency of 24 Hz. This data was processed using SEASOFT Ver 4.207 provided by Sea-Bird Electronics Inc. and some programs developed in JAMSTEC coded in FORTRAN (Microsoft FORTRAN compiler was used).

We report temperature and salinity value from primary sensors, pressure value from pressure sensor in WOCE-CTD-file, although we used twin temperature and conductivity sensors, pressure sensor, and DO sensor. We used the result from secondary sensors to check up one from primary sensors. We don't report the result from DO sensor because we haven't established calibration method of DO-sensor.

We don't also report the data when CTD was near surface (upper than 15 db) because the pump of CTD was not active then.

CTD-file are created using downcast CTD data. We used upcast CTD data for data check and calculation of CTD T/S/P value in WOCE-SEA-file.

Pre-cruise and post-cruise calibration for temperature and conductivity sensors were carried out at NRCC (Northwest Regional Calibration Center) in USA on 23 April 1996 and 31 August 1996. Pre-cruise and Post-cruise calibration for pressure sensor by dead weight tester was carried out at JAMSTEC on 6 June 1996 and 4 October 1996. We check up and calibrated CTD data considering these result.

a. Seagoing computer

We used 3 computer systems for data processing as follows:

(1) System 1 (for data acquisition)

CPU: DECpc 466D2LP (IBM compatible computer, MS-DOS Ver.5)

with 8MB memory, 240MB hard disk and 3.5-inch floppy disk drive.

Optical disk: 3.5-inch and 5-inch optical disk drives.

We used 3.5-inch optical disk during data processing and 5-inch optical disk for backup of raw data from CTD deck unit.

Other: This system is connected with deck unit.

(2) System 2 (for data processing)

CPU: DECpc 466D2LP

with 8MB memory, 240Mb hard disk, 3.5-inch floppy disk drive and 5-inch floppy disk drive.

Optical disk: 3.5-inch optical disk drive.

Plotter: Hewlett Packard 7475A Plotter (Paper size is A4)

Hard disk: two 2GB hard disk drives.

(3) System 3 (for data editing)

CPU: NEC PC9821 NA12 (Windows95)

with 32MB memory, 1.2GB hard disk, CD-ROM drive and 3.5-inch floppy disk drive.

Optical disk: 3.5-inch optical disk drive.

b. Data processing

(1) General

In order to remove white noise in raw temperature, conductivity and pressure data, we developed software that replaced noise data by running mean. We defined the noise as shown in table C.3-1. Few noises in pressure data over this criteria were detected because of the short period of oscillation (see later).

Shed wakes, which occurred in the case of CTD decent rate being slow or reversal because of the pitch of the ship, were removed using the program developed in JAMSTEC. This program (FDSHDWK) finds shed wakes when CTD decent rate is less than 0.25 m/s and linearly interpolates pressure, temperature and conductivity values in the shed wake using its upper and lower values. If the number of the interpolated values is more than half of the number of observations in some 2db pressure bin, its quality flags of pressure, temperature and salinity should be 6 in CTD file.

After all on-board calibration, uniform pressure CTD profile data was created by same method as one of Millard and Yang (1993).

(2) Temperature

The results of laboratory calibrations for temperature sensors show that CTD temperature sensor tend to drift constantly with time. The difference between

twin temperature sensors was almost constant. The result from pre- and post-cruise calibration carried out on 23 April and 31 August shows that the drift of the primary temperature sensor was -0.0010 (deg C). Considering these result, we could estimate that offset correction added to the value of primary temperature sensor was +0.0005 (deg C) during this cruise.

Laboratory calibration carried out on IPTS-68 unit, we converted raw temperature value on IPTS-68 to ITS-90 unit using formula (3) of Millard and Yang (1992) after the offset correction.

(3) Conductivity(salinity)

Conductivity value was corrected as follows:

Step 1. Sensor response correction.

According to Millard and Yang (1993), salinity spikes are caused by sensor response lag between temperature and conductivity. We checked this time lag between T and C sensors for SBE 911 plus system and determined it when total salinity spike area (S) defined as follows was minimum.

$$S = \sum_{i=1}^N (P_{Li} - P_{Ui}) H_i.$$

N is the number of spike, P is pressure, H is height of spike and suffix U and L mean upper and lower boundary of spike. Fig.C.3-1 is result at the test cast conducted before 8S-01. The results show that time lag should be 0.4 steps, that is, 0.0167 seconds. We used ALIGNCTD of SEASOFT for this correction throughout this cruise.

Even if sensor response correction is done, the salinity spikes still remain. When we find a salinity spike lager than 0.01 PSU in some 2db pressure bin, quality flag of salinity should be 3 in CTD file.

Step 2. Cell thermal mass correction.

Sea-Bird Electronics Inc. recommend that conductivity cell thermal mass effect should be removed. We used CELLTM of SEASOFT to remove this effect.

This utility uses recursive filter described in Lueck (1990).

Step 3. Cell factor correction.

We used Autosal to calibrate CTD conductivity sensor. We determined cell factor by linear regression between CTD conductivity when bottle was fired and conductivity of sampled water measured by Autosal for every casts. CTD conductivity was corrected using the equation as follows:

$$C_{\text{calibrated}} = A \times C_{\text{raw}} + B.$$

A and B are slope and offset, respectively.

(4) Pressure

The result of pre-cruise calibration conducted on 4 June by dead weight tester is shown in Fig.C.3-2 . It indicates that the difference between CTD and dead weight tester values was linearly increased. This difference is corrected by regression line with slope and offset of 0.99899 and 5.15870. The error from the approximation using this regression is lower than 0.2 db. The slope and offset shifted to 0.99901 and 4.88735 at 2 October. The estimation of shift of pressure value using these result is 0.3 db between pre-cruise and post-cruise. We do not correct this shift.

The pre- and post-cruise calibration result also showed that hysteresis is 0.1 db. This error is not also corrected.

Raw data from pressure sensor has short period (<0.2 seconds) oscillation. We used FILTER of SEASOFT and filtered this oscillation by low pass filter that time constant was 0.15 seconds.

The variability of deck pressure was shown in Fig.C.3-3. The deck pressure is increased up 0.4 - 1.0 db after cast. CTD pressure value is subtracted by the average of the deck pressure before and after cast.

c. Data flow

(See Fig.C.3-4)

(1) SEASAVE (SEASOFT)

Acquires, displays and saves raw data from deck unit to disk.

(2) DATCNV (SEASOFT)

Converts raw, binary data output by SEASAVE to ASCII format data written on physical unit. When water is sampled, this program can output data to .ROS file from that time after a few seconds. (On this cruise, this interval was 10 seconds.)

(3) ROSSUM (SEASOFT)

Edits .ROS file output by DATCNV and writes out a summary file to .BTL file.

(4) BT2FILE (Made in JAMSTEC)

Changes the format of .BTL data to another format for convenience.

(5) SPLDEP (Made in JAMSTEC)

Splits ASCII format data by DATCNV into up- and downcast data, and calculates deck pressure and corrected depth values.

(6) TCCOMP (Made in JAMSTEC)

Compares values of primary and secondary sensors, and plots histograms to check sensor's performance.

(7) NOISE (Made in JAMSTEC)

Finds noise data and replaces it by running mean. This program can remove unnecessary surface data.

(8) ALIGNCTD (SEASOFT)

Corrects time lag between temperature sensor and conductivity sensor for minimizing salinity spiking error.

(9) FILTER (SEASOFT)

Uses low pass filter to remove short period oscillation in pressure data.

(10) CELLTM (SEASOFT)

Corrects conductivity cell thermal effect using a recursive filter.

(11) FDSHDWK (Made in JAMSTEC)

Finds shed wake and interpolates data using the values of its upper and lower boundary.

(12) FSPIKE (Made in JAMSTEC)

Finds salinity spike.

(13) CALBC (Made in JAMSTEC)

Calibrates conductivity data by cell factor correction. This program also corrects the temperature sensor drift and deck pressure of the CTD data reported

in WOCE-SEA file.

(14) AVGDAT (Made in JAMSTEC)

Calculates 2db pressure averaged data. After averaging, this program corrects the temperature sensor drift and deck pressure of the CTD data.

(15) MKCTD (Made in JAMSTEC)

Creates WOCE-CTD file.

d. Conclusion

We could acquire high quality CTD data satisfying WOCE requirement except for the bin where salinity spikes and shed wakes were. Estimated accuracy of CTD pressure, temperature and salinity is as follows:

(1) Pressure

Considerable error of CTD pressure value is 1) 0.2 db from regression, 2) 0.3 db from the shift from pre-cruise to post-cruise, 3) 0.1 db from hysteresis, and 4) 0.4 db from deck pressure variability. Therefore, accuracy of CTD pressure value is 1 db during P8S cruise.

(2) Temperature

Accuracy of temperature value should be 0.001 K because the drift of temperature sensor shown by pre- and post-cruise calibration is 0.0010 K, and twin sensor check shows that primary temperature sensor performed satisfactorily.

(3) Salinity

Comparison between CTD salinity and sampled water salinity is shown in Table C.3-2. This result implies that the accuracy of CTD salinity is higher than 0.001 PSU below 500 db.

References

- 1) Millard, R., and K. Yang: CTD calibration and processing methods used at Woods Hole Oceanographic Institution, WHOI Tech. Rep. 93-44, 1993.
- 2) Lueck, R.: Thermal Inertia of conductivity cell: Theory, J. Atmos. Oceanic Technol., 7, 741-755, 1990.

Table C.3-1. Definition of noise

	Pressure (db)	Temperature (deg C)	Conductivity (S/m)
1. Range	0.5 < or 8000 >	0 < or 32 >	2 < or 8 >
2. Difference from value in a previous step value	1.0 >	0.5 >	0.05 >
3. Difference from running mean			
(a) 0 - 400m	0.5 >	1.0 >	0.1 >
(b) 400 - 1000m	0.5 >	0.2 >	0.02 >
(c) 1000 - 2000m	0.5 >	0.1 >	0.01 >
(d) 2000 - bottom	0.5 >	0.05 >	0.005 >

Table C.3-2. Average, root mean square and maximum of absolute value of the difference between CTD salinity and Autosal salinity

depth (db)	average (PSU)	RMS (PSU)	maximum (PSU)	No. of sample
0 - 500	-0.00582	0.02771	0.1802	307
500 - 2000	-0.00020	0.00081	0.0046	247
2000 - bottom	0.00014	0.00057	0.0018	325

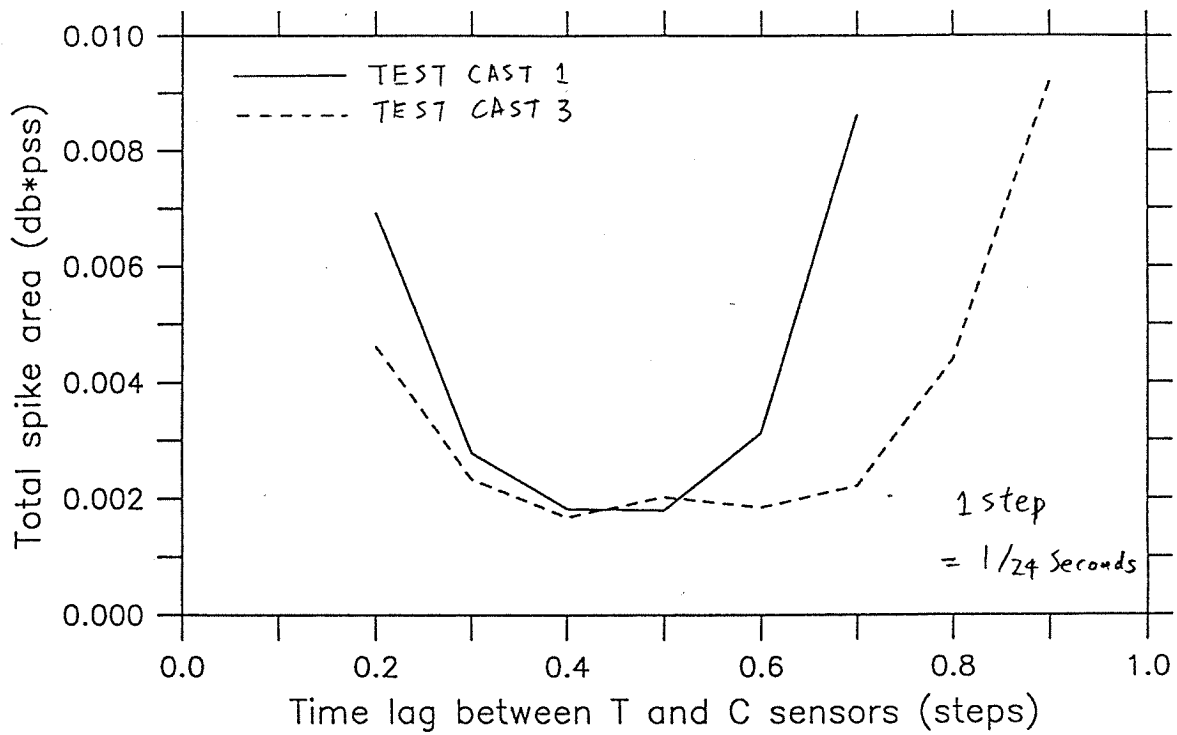


Fig. C.3-1. Total salinity spike area variability for time lag between T and C at the test cast 1 (solid line) and 3 (broken line).

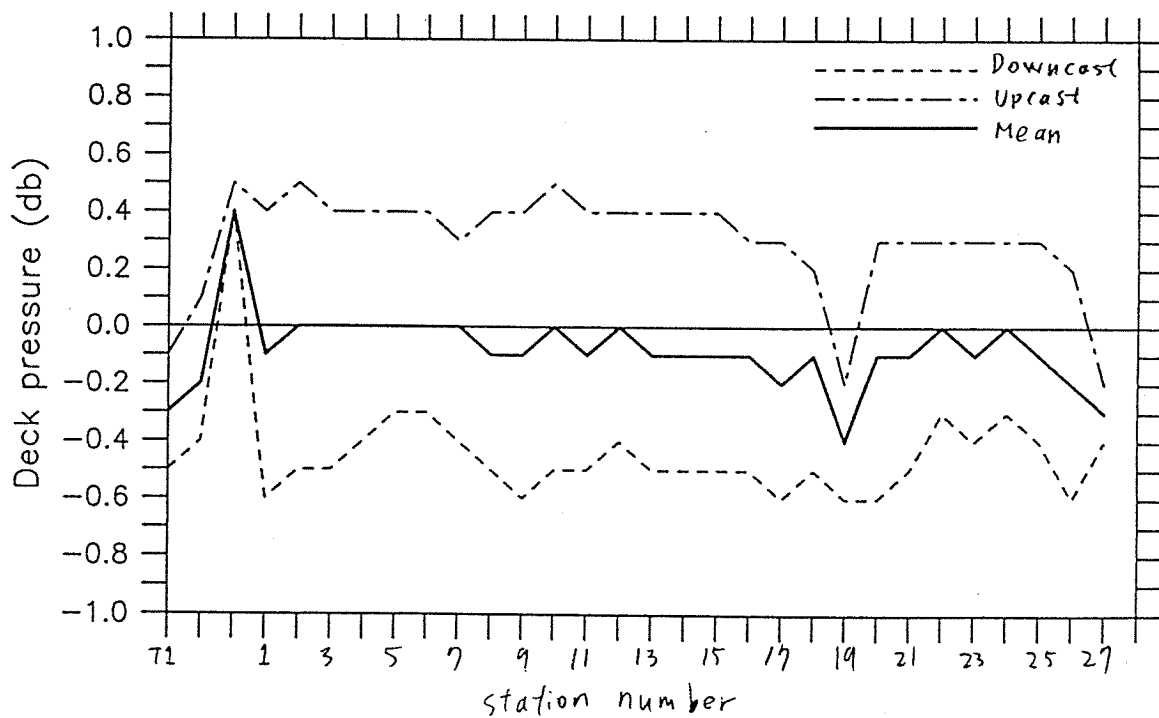


Fig. C.3-2. Deck pressure variability during P8S cruise.

Result Of D. W. T.
SBE 9puls S/N 0319

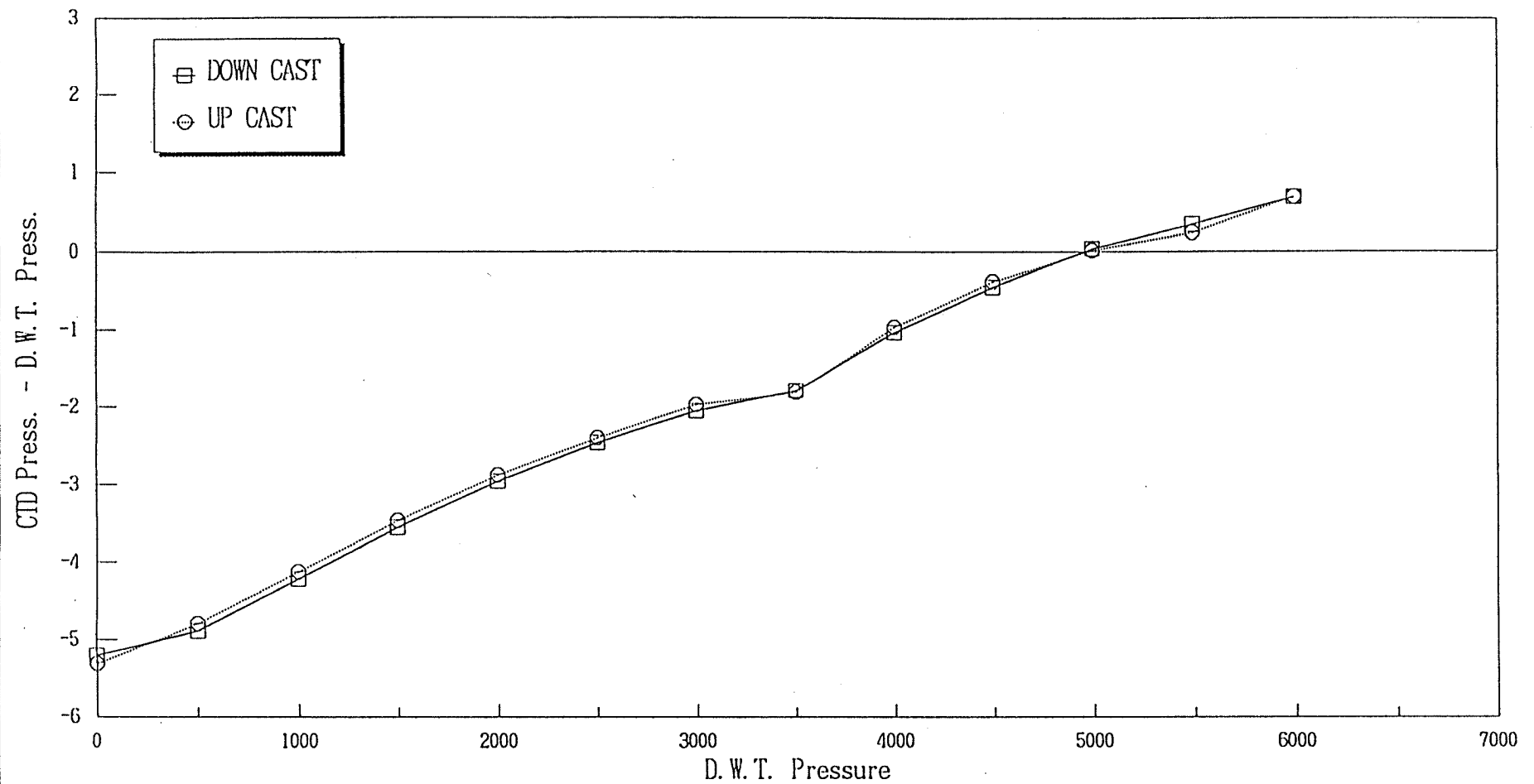


Fig. C.3-3. Result of pressure sensor calibration using a dead weight testor.

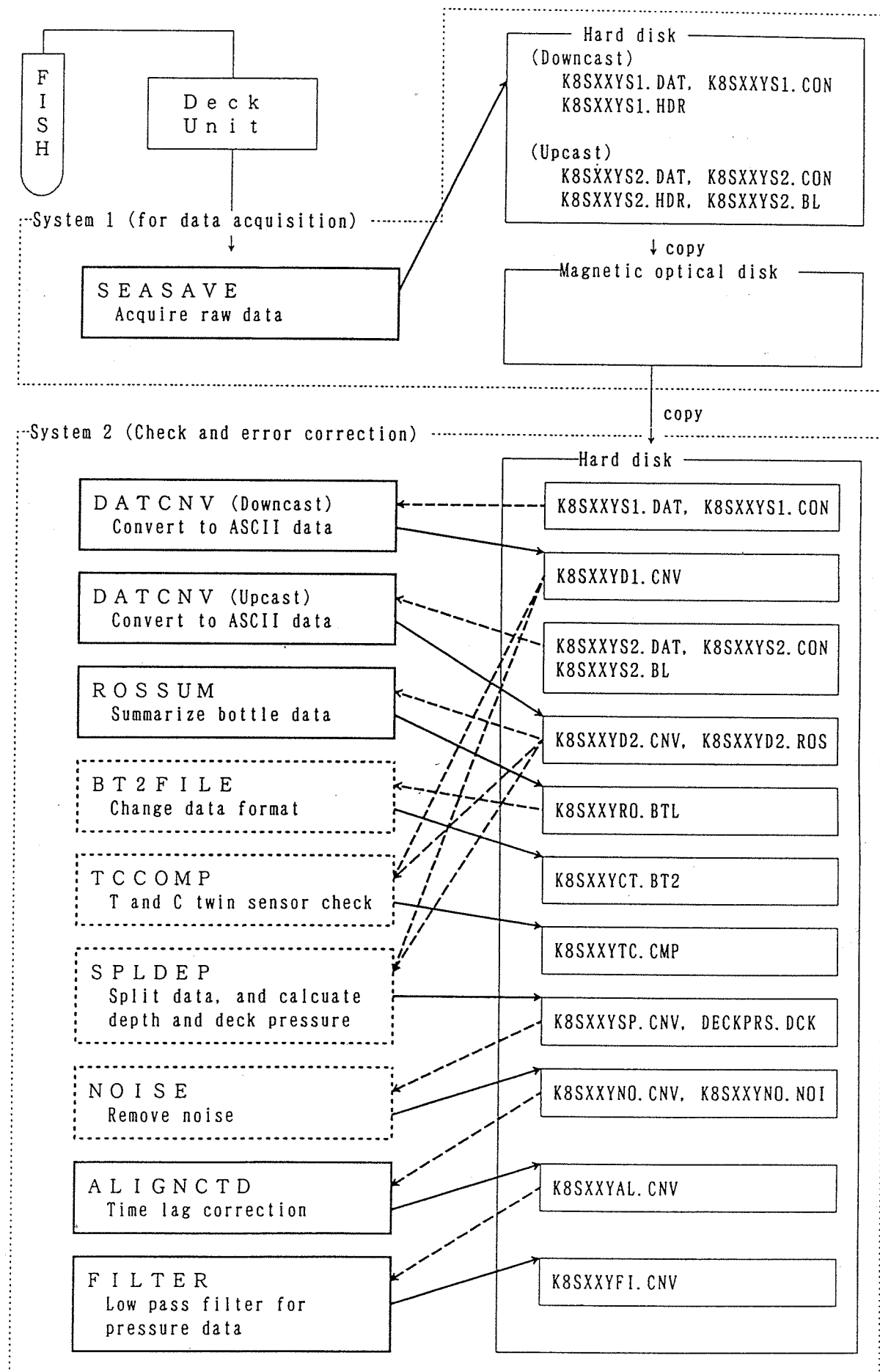
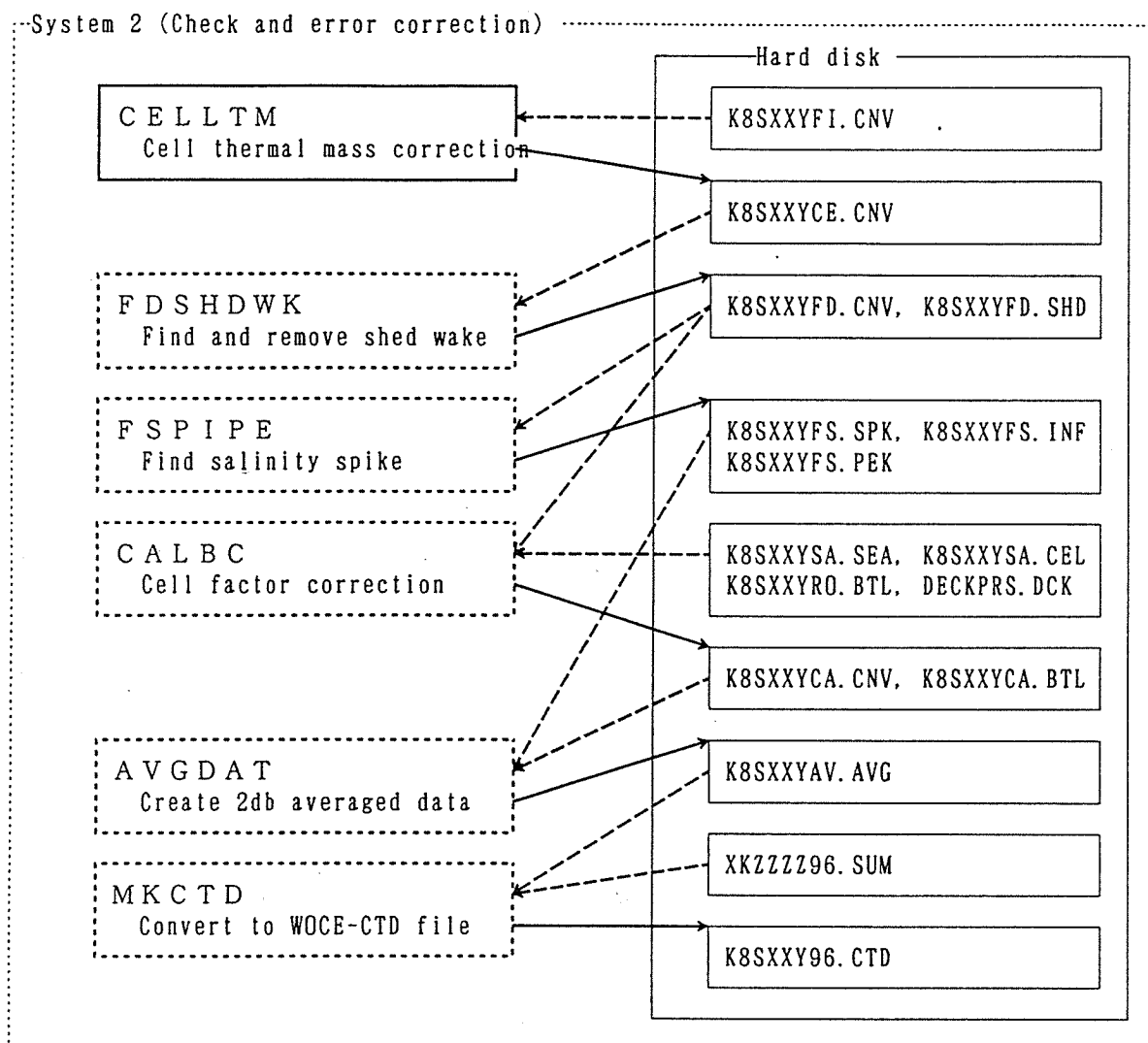


Fig. C.3-4. Data flow of CTD data processing.



XX and Y in the file name denote station number and cast number, respectively.

Fig. C.3-4. (Continued)

C.4 Sample water salinity measurements

by H. Yoritaka, A. Ito and M. Hayashi (September 1996)

1. Salinity Sample Collection

The bottles in which the salinity samples are collected and stored are 250ml Phoenix brown glass bottles with screw caps. Each bottles were rinsed three times and filled with sample water. Salinity samples were stored for about 24 hours in the same laboratory as the salinity measurement was made.

2. Instruments and Method

The salinity analysis was carried out by a Guildline Autosol Salinometer model 8400B, which was modified by addition of an Ocean Science International peristaltic-type sample intake pump and Hewlett Packard quartz thermometer model 2804A with two 18111A quartz probes. One probes measured an ambient temperature and another probe measured a bath temperature. The resolution of the quartz thermometer was set to 0.001 deg C. Data of both the salinometer and the thermometer was collected simultaneously by a personal computer. A double conductivity ratio was defined as a median of 31 readings of the salinometer. Data collection was started after 5 seconds and it took about 10 seconds to collect 31 readings by a personal computer.

The salinometer was operated in the airconditioned ship's laboratory at a bath temperature of 27 deg C. An ambient temperature varied from approximately 25 to 26 deg C, while a variation of a bath temperature was almost within ± 0.004 deg C.

3. Standard Sea Water

Autosal model 8400B was standardized only before sequence of measurements by use of IAPSO Standard Seawater batch P128 whose conductivity ratio was 0.99986. After the standardization, 8400B was monitored by 1-4 SSW ampules before and after the measurements for samples of one station. Total 61 ampules of SSW were measured for monitoring, whose standard deviation was 0.0005 psu. There was slight drift for 8 days (from June 24 to July 1) in monitoring of SSW, so correction was carried out for sample measurements as follows ;

Station 01-15 : Corrected Value = Measured Value -0.0000 psu (0 digit)

Station 16-20 : Corrected Value = Measured Value -0.0002 psu (1 digit)

Station 21-27 : Corrected Value = Measured Value -0.0004 psu (2 digits)

After correction, standard deviation for SSW was slightly improved as 0.0004 psu.

4. Duplicate and Replicate Samples

Duplicate samples were drawn from Niskin bottles #1 and #2 which were tripped at the bottom, and also drawn from different Niskin bottles which were tripped at 1000 db in case of shallower water depth than 5000 m. Replicate samples were drawn from Niskin bottles #2. Standard deviation in the measurements of duplicate and replicate samples were as follows ;

Duplicate	Bottom 0.0002 psu	26 pairs
	1000 db 0.0002 psu	14 pairs
Replicate	Bottom 0.0001 psu	25 pairs.

C.5 Dissolved Oxygen determination

by M. Aoki , T. Shiribiki and M. Fujisaki (19, August, 1996)

Methods:

Oxygen samples were collected from Niskin bottles to calibrated dry glass bottles , and sample water were overflowed by three times of the bottle volume. The subsampling bottle consists of the ordinary BOD flask (ca. 200 ml) and glass stopper with long nipple, modified from the nipple presented in Green and Carritt(1966).

Dissolved oxygen in seawater samples were fixed immediately following the water temperature at the time of collection was measured for correction of the sample density. Samples were analyzed about 2 hours later. The end point was determined by the potentiometric method using whole bottle titration. We used 2 sets of Metrohm titrators with automatic burettes and Pt electrode (titrator #1 and #2) for DO. measurements. The average water temperature in the laboratory was 22.8 °C, while room temperature varied in several minutes between 20 to 27 °C.

The standardization was done for each stations and whenever the batch of reagents were changed. An analytical method was fundamentally done according to the WHP Operations and Methods (Culberson,1991). The endpoint was evaluated by the second-derivative curve method with computerization.

Instrument:

Dispenser : Eppendorf Comforpette 4800 / 1000 μ l

OPTIFIX / 2 ml

Metrohm Model 725 Multi Dosimat / 20 ml

Titration : Metrohm Model 716 DMS Titrino / 10ml of titration vessel

Pt Electrode / 6.0403.100(NC)

Software : Data acquisition / Metrohm, METRODATA / 606013.000

Endpoint evaluation / written by N88BASIC / MS-DOS

(NEC / P9821ne, PC9821na)

Thiosulfate Standardization :

We used 3 batches of KIO₃ standard solutions (JM960612, JM960613 and CSK KCP8418 : see note below Table C.5-1). Standardization was carried out at

each station except for stns. 6, 11, 19 and 26. The results using JM960612 KIO3 solution were that the average of 1.4016 ml (titrator #1) and 1.4038 ml (titrator #2) and standard deviation of 0.0025 ml (#1) and 0.0016 ml (#2) (Fig. C.5-1).

Pure water blanks :

The pure water blanks were determined in deionized water (by Milli-RX12, Millipore). The results of the pure water blanks were that the average of -0.0092 ml(#1) and -0.0093 ml(#2), and standard deviation of 0.0014 ml(#1) and 0.0015 ml(#2)(Fig. C.5-2).

Dissolved Oxygen in the reagents :

DO. in the reagent was reported 0.0017 ml at 25.5 ° C (Murray et. al., 1968). Last cruise, in 1995, we estimated the amount of dissolved oxygen in the reagents that was 0.0027 ml at 21 ° C. In this cruise, we used 0.0027 ml DOrea value for calculation.

Seawater blank :

In this cruise, we analyzed 69 samples for determination of seawater blanks. Most of samples were taken from the layer of 10m, oxygen minimum and bottom at each station. The result shows wide range of blank value and they are not depended on the depth.

Average of seawater blank was 0.08 $\mu\text{mol/Kg}$ and standard deviation (2sigma) was 0.58 $\mu\text{mol/Kg}$ (cf. Fig. C.5-6b). Dissolved oxygen concentrations for the SEA file were not corrected by water blank.

Reproducibility :

In this cruise, 1027 samples were taken for dissolved oxygen measurements. Approximately 14% (148 pairs) of total samples were analyzed as "replicates" taken from same Niskin bottles. And 39 pairs of duplicate samples were analyzed throughout this cruise. Those results are shown in Fig. C.5-3 and Fig. C.5-4.

Replicates sample, 148 pairs, were obtained average of 0.004 $\mu\text{mol/kg}$ and standard deviation (2 sigma) of 0.52 $\mu\text{mol/Kg}$ (0.25 % of DO. maximum, 204.1 $\mu\text{mol/Kg}$, in this cruise). Duplicate sample, 39 pairs, were taken from different

Niskin bottles fired at the same depth (26 pairs from the bottom layer, 12 pairs from 1000m and 1 pair from 900m layer). The average difference among them was 0.09 $\mu\text{mol/Kg}$, and standard deviation (2 sigma) was 0.42 $\mu\text{mol/Kg}$ (0.21 % of DO. maximum in this cruise).

Comparison of each standard:

Before the cruise, we compared each standard. The results are shown in Table C.5-1.

Table C.5-1. Comparison of each standard.

<u>KIO3 Lot No.</u>	<u>Normality</u>	<u>average titer</u>	<u>std.</u>	<u>cv %</u>	<u>n</u>	<u>Ratio to CSK Std.</u>
CSK KCP8418	0.0100	1.396 (ml)	0.001	0.05	5	1.0000
JM960612	0.010014	1.397 (ml)	0.001	0.06	5	0.9997
JM960613	0.010014	1.398 (ml)	0.001	0.07	5	1.0005
CSK AMP8047	0.0100	1.396 (ml)	0.000	0.03	5	1.0000

Note : CSK KCP8418 and AMP8047 are the commercially standard solution prepared by Wako pure chemical industries, Ltd. (Guaranteed by Chemical Research Center)

Comparison of standards from other institution:

In this cruise we compared 2 types of standard solution. One is JM which had prepared before this cruise and the other is HDJ (Hydrographic Department, Maritime Safety Agency, Japan) which had been stored since 1994. Standard solution named JM960602 and JM960612 were prepared before this cruise but JM960602 had been weighed in Nov. 1993. The standard solution labeled HDJ02 was stored under the room temperature, but HDJ03 was in a refrigerator either HDJ04 was. Standard HDJ04 was diluted from nominal concentration 0.1 N to 0.01 N before the cruise. We measured these standards on board using the same titration system and reagents. The results are shown in Table C.5-2.

Table C.5-2. Comparison of standards between JAMSTEC and HDJ.

KIO3 Lot No.	Normality	average titer	std.	cv%	n	Ratio to JM960612
JM960602	0.010034	1.402	0.0026	0.19	6	1.0008
HDJ02	0.0100	1.392	0.0009	0.07	5	0.9967
HDJ03	0.0100	1.392	0.0008	0.05	5	0.9970
HDJ04	0.00998	1.405	0.0005	0.04	5	1.0078
JM960612	0.010014	1.398	0.0008	0.06	5	1.0000

Comparison with historical data:

This P8S cruise line and PR1S cruise line which carried out in 1994 were lined along longitude 130°E. There were 14 stations in the same latitude on this line. Dispensers, except for the Eppendorf, and electrodes were changed between these 2 cruises.

DO. concentration

Table C.5-3 shows the differences of dissolved oxygen concentration between P8S and PR-1S every 1000m below 3000m. The difference between them are obtained to 0.2 - 0.5% of DO.

Table C.5-3. Comparison of DO. concentration between PR-1S and P8S.

Range (m)	PR-1S,1994 μmol/kg	std.	P8S, 1996 μmol/kg	std.	Ratio of difference to DO. in 1994(%)
3000 - 4000	148.3	3.23	147.5	3.40	-0.5
4000 - 5000	151.7	0.87	152.0	0.82	0.2
5000 -	151.7	0.88	152.5	0.40	0.5

Note; DO. concentrations are the average within a range. of Those data are not corrected by seawater blank.

For example, Fig. C.5-5a and C.5-5b show the differences of profile at the same latitude. DO. concentrations above 1000m may show the replace of the water mass.

Seawater blank

We measured seawater blanks from some layers at each station both in 1994 and 1996 cruises. The results are shown in Table C.5-4. In both cruise, the values of seawater blank varied independently of their sampling depth. The methods of analyses were almost the same as for seawater samples but no fixation.

Table C.5-4 . Comparison of seawater blank calculated to DO. concentration.

Line name	seawater blank umol/kg	std.	n
PR-1S, 1994	1.09	0.64	55
P8, 1996	0.08	0.29	69

References :

- Culberson, C.H. (1991) Dissolved Oxygen, in WHP Operations and Methods, Woods Hole., pp1-15.
- Culberson, C.H., G.Knapp, R.T.Williams and F. Zemlyak (1991) A comparison of methods for the determination of dissolved oxygen in seawater (WHPO 91-2), Woods Hole.
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- Green, E.J. and D.E.Carritt (1966) An Improved Iodine Determination Flask for Whole - bottle Titrations, Analyst, 91, 207-208.
- Murray, N., J.P. Riley and T.R.S. Wilson (1968) The solubility of oxygen in Winkler reagents used for the determination of dissolved oxygen, Deep-Sea Res., 15, 237-238.

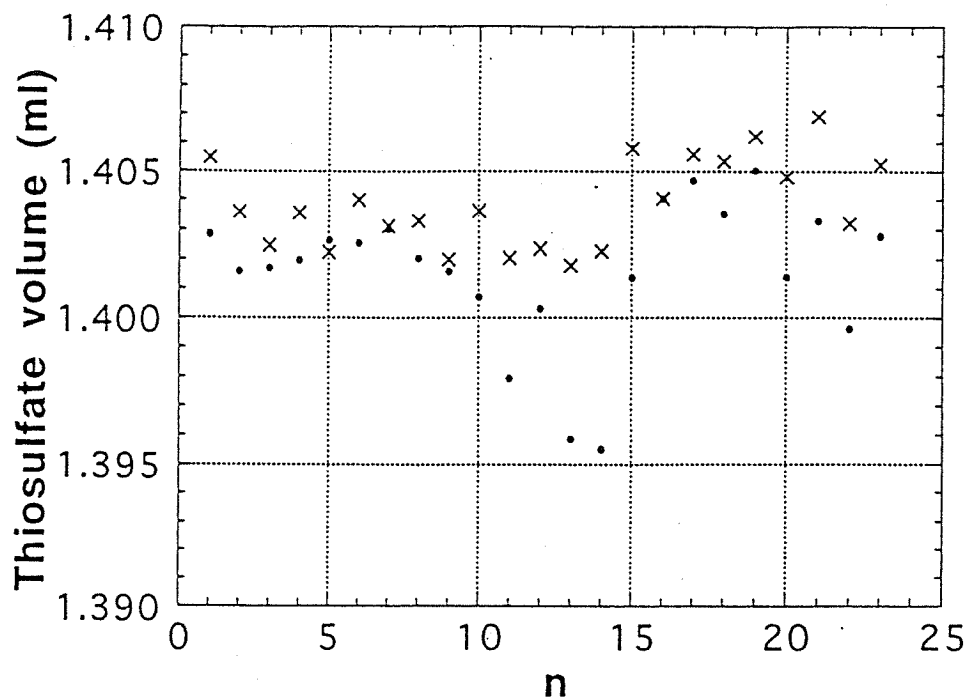


Fig.C.5-1 Results of thiosulfate standardization.
 Dot shows titrator #1 and cross shows #2.

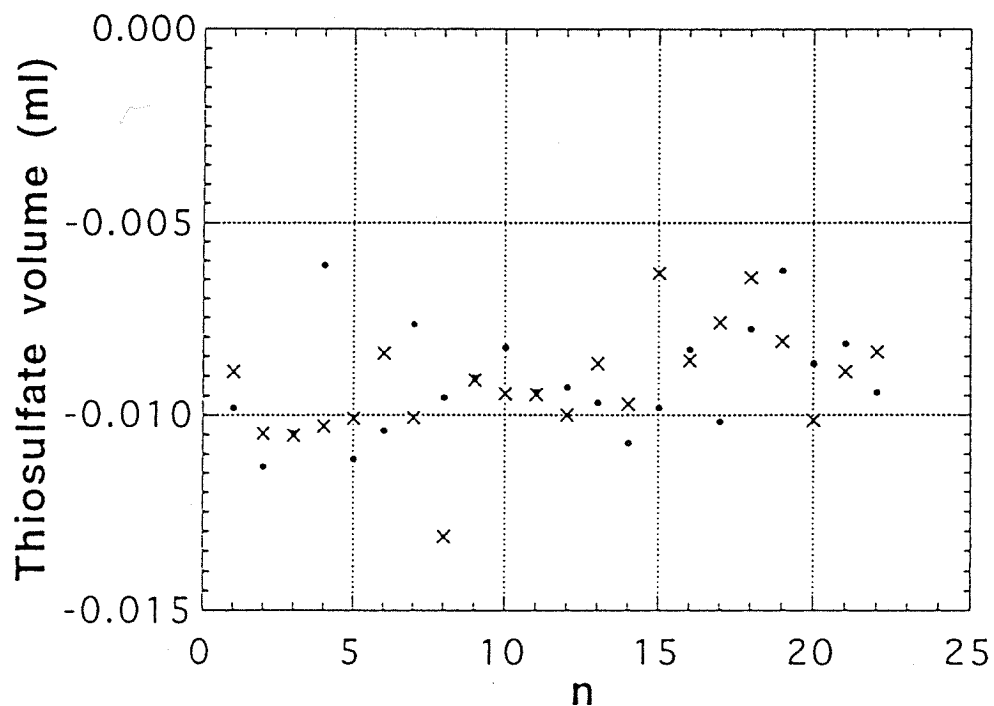


Fig.C.5-2 Results of purewater blank with KIO3 standard solution JM960812. Dot shows titrator #1 and cross shows #2.

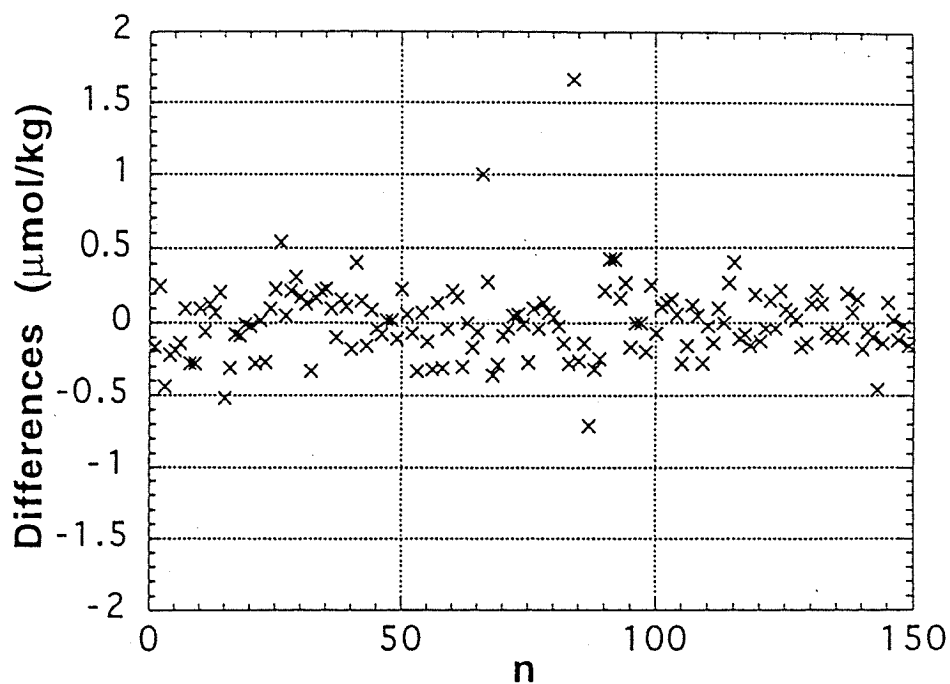


Fig.C.5-3 Differences between "Replicate" samples.
 average=0.004μmol/kg, std(2σ)=0.52μmol/kg,
 0.25% of D.O. max.

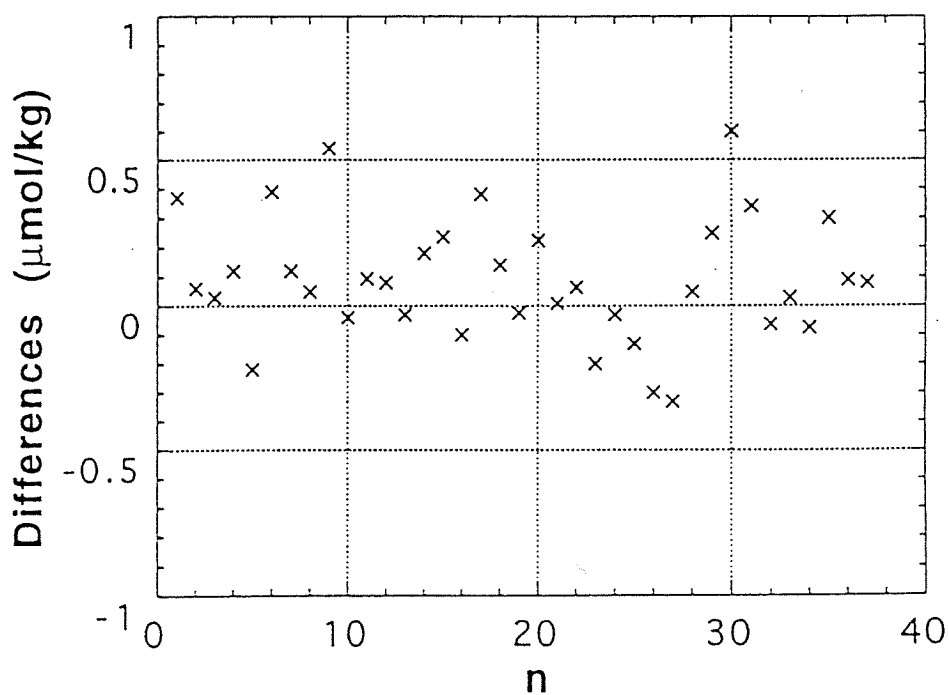


Fig.C.5-4 Differences between "Duplicate" samples.
 average=0.09μmol/kg, std(2σ)=0.42μmol/kg,
 0.21% of D.O. max.

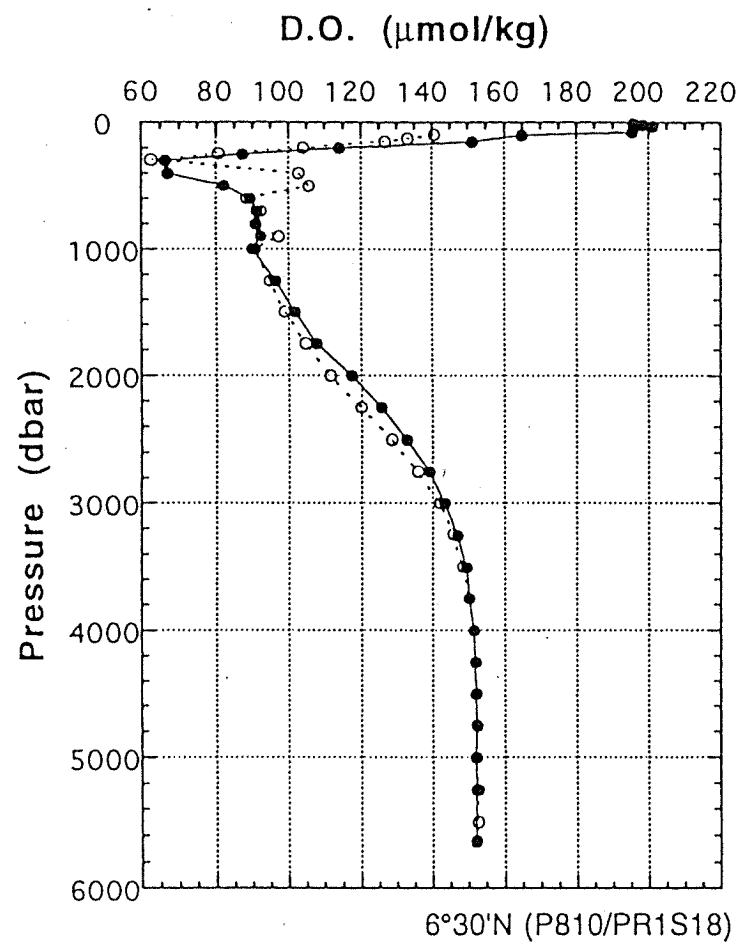


Fig.C.5-5a Profile of D.O. concentrations at 6°30'N. Solid circle shows the results in 1996 and open circle is in 1994.

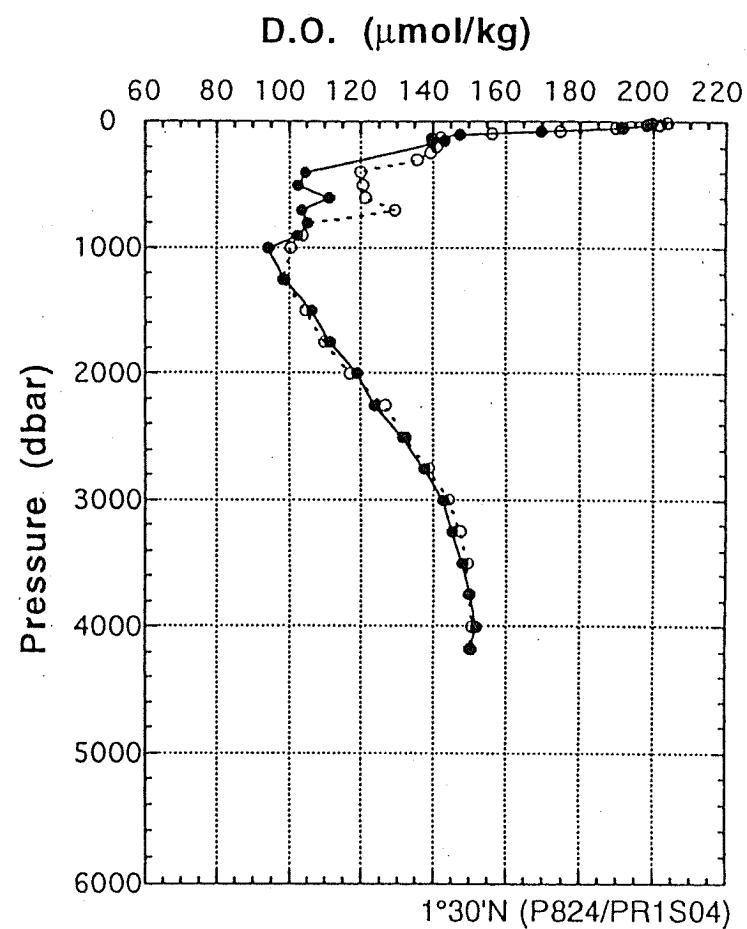


Fig.C.5-5b Profile of D.O. concentrations at 1°30'N

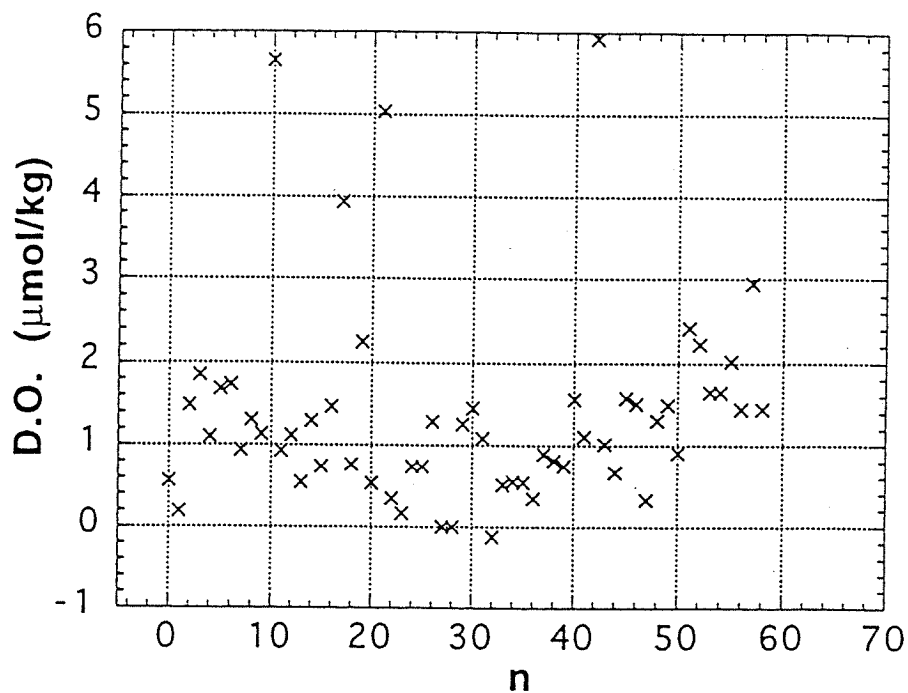


Fig.C.5-6a Seawater blanks in PR-1S, 1994.
 average= $1.09\mu\text{mol/kg}$, std= $0.64\mu\text{mol/kg}$,

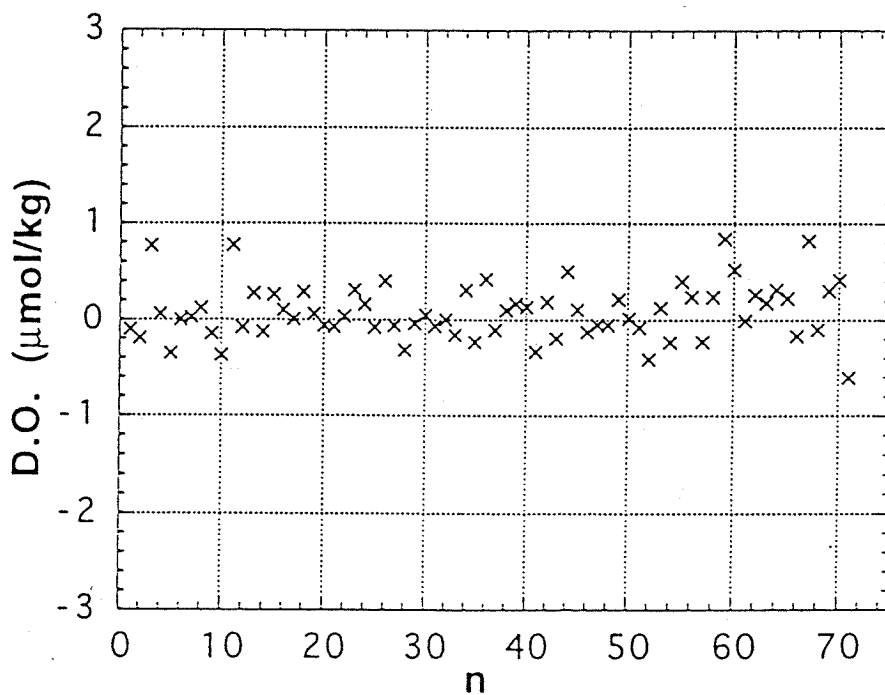


Fig.C.5-6b Seawater blanks in P8S, 1996.
 average= $0.08\mu\text{mol/kg}$, std= $0.29\mu\text{mol/kg}$,

C.6 Nutrients measurements

by Y. Nogiwa, K. Nakao, N. Komai and C. Saito (July, 1996)

a. Equipment and techniques

The nutrients analyses were performed on BRAN+LUEBBE continuous flow analytical system Model TRAACS 800 (4 channels). The manifolds for the analysis are shown in Fig. C.6-1, -2, -3 and -4 for the nitrate+nitrite, nitrite, silicate and phosphate, respectively. TRAACS 800 was located in the container laboratory on deck the R/V Kaiyo.

The methods used were as follows:

1st channel

Nitrate+Nitrite: Nitrate in seawater is reduced to nitrite when a sample is run through a cadmium tube (1 mm diameter, 10 cm length) inside of which is coated with metallic copper. The nitrite produced is determined by diazotizing with sulfanilamide and coupling with N-1-naphthyl- ethylenediamine (NED) to form a colored azo dye which is measured spectrophotometrically at 550 nm using 3 cm length cell. Nitrite initially present in the sample is corrected. Since the reduction rate was varied from 92 to 97 %.The reduction rate was measured for each analysis and the concentration of nitrate was corrected by reduction rate.

2nd channel

Nitrite: The nitrite is determined by diazotizing with sulfanilamide and coupling with N-1-naphthyl- ethylenediamine (NED) to form a colored azo dye which is measured spectrophotometrically at 550 nm using 5 cm length cell.

3rd channel

Silicate: The standard AAII molybdate-ascorbic acid method with the addition of a 46 deg C heating bath to reduce the reproducibility problems encountered when analyzing samples at different temperatures. The silicomolybdate produced is measured spectrophotometrically at 630 nm using 3 cm length cell.

4th channel

Phosphate: The method of Murphy and Riley (1962) was used, but separate

additions of ascorbic acid and mixed molybdate-sulfuric acid-tartrate and addition of a 46 deg C heating bath. The phosphomolybdate produced is measured spectrophotometrically at 880 nm using 5 cm length cell.

The analytical results were corrected for base drift, carry over effect and gain drift. The concentrations of nitrate+nitrite, nitrite, silicate and phosphate were calculated by 2nd order polynomial curve fitting. The temperature of all sample seawater at the analyses was measured and recorded. The temperature of the sample seawater during this cruise ranged from 16 deg C to 26 deg C depending on duration of analysis and ambient temperature.

b. Sampling Procedures

Sampling for nutrients followed that for oxygen. Samples were drawn into polyethylene 100 ml narrow mouth, screw-capped bottles. These were rinsed two to three times before filling. Most of the samples were analyzed within 4 hours after collection. Glass 7 ml sample cups were used. Glass cups were washed in the hot detergents, they were rinsed by deionized water, and kept in deionized water before packing. These were rinsed two times before filling with analyze.

c. Calibration

The calibration of all the volumetric flasks used on the cruise were checked before packing. Calibration of the 3 Eppendorf micropipettes used during the cruise were checked before packing. The temperature during the calibration ranged from 21 to 23 deg C.

d. Nutrient standard

We prepared nutrient standards by following "an suggested protocol for continuous flow automated analysis of seawater nutrients" by Gordon et.al (1992). Nutrient primary standards of nitrate, nitrite and phosphate were prepared from salts dried in oven/microwave oven and cooled over silica gel in a desiccator before weighing. The dry powder for the primary standard was packed in the nitrogen gas atmosphere. The precision of the weighing was ca. 0.1 %.

Silica standard (one gram of SiO₂ in plastic ampule, comm No. 4790) prepared by J.T. Baker Chemical Co. was used to prepare the standard solution of silicate

analysis during this cruise.

The concentration of A standard are 2500 μM for phosphate, 37500 μM for nitrate and 3800 μM for nitrite, and 33286.6 μM for silicate. The concentration of B standard are 50 μM for phosphate, 750 μM for nitrate and 38 μM for nitrite, and 2662.9 μM for silicate. A and B uniform set of six mixed working standards were prepared in low nutrients sea water (LNSW). Concentrations ($\mu\text{mol/l}$) were: nitrate 45.0, 37.5, 30.0, 15.0, 7.5 and 0 ; nitrite 1.2, 1.0, 0.8, 0.4, 0.2, and 0; silicate 162, 135, 108, 54, 2.7 and 0 ; phosphate 3.0, 2.5, 2.0, 1.0, 0.5 and 0 thereafter.

e. The traceability of the standard

Two sets of A standards were prepared at the beginning of the cruise. One of two was used for 15 of working standard during the cruise. The other was stocked as reference A standard to be checked the working standard. The results of this check are shown in Table C6-1.

f. The comparison between working standard solution and CSK standard solution at full scale.

The comparison between working standard solution and CSK standard solution at full scale were made three times before the cruise and once after cruise onboard.

g. Low nutrient sea water

More than 200 liter of surface seawater was collected in JUNE 1995 near Palau Is. as low nutrient seawater (LNSW). Collected seawater was stored in the 20 liter container and filtered with 0.45 μm pore size membrane filter (Millipore HA) and subjected to prepare the working standard solution. The concentration of nutrients in each batch of LNSW were determined carefully.

h. Experiment for preparation of Control sample

Control samples were prepared to confirm traceability in the nutrients measurements during the cruise and examined the availability of it.

Method of control samples were :

Sea water (31°N, 133°E, 2500 m) was sterilized heating at 120 deg C for 30 minuets twice after it had been filtered with 0.45µm(Millipore HA)and 0.22µm(MILLIPACK 40)pore size membrane filter. Then the sea water was drawn into sterilized 100ml polypropylene bottles under aseptic condition over filtering with 0.22µm pore size membrane filter again. We confirmed that the control samples condition were free from bacteria and fungi. The 37 control samples were measured. One each analysis,one more bottle control samples were analyzed five times a bottle. The measurement results are in table C.6-4

i. Precision check at each station

On each analysis, one of the deep water sample and one of the shallow water sample were analyzed five times to get the precision, respectively. The precision at full scale at each station were shown in Table C.6-5.

j. Replicate and Duplicate Samples

There were 27 pairs of replicate and duplicate samples drawn. We drawn 2 samples from the Niskin bottles tripped at the bottom for a replicate and 1 sample from another Niskin bottle tripped at the bottom for a duplicate. The standard deviation of 27 pairs of replicate and duplicate samples were 0.0005 PSU.

Table C.6-1. The concentration ratio of working standard solutions referenced to stocked A standard solution.

Date	Nitrate	Nitrite	Silicate	Phosphate
19 June '96	1.008	1.008	1.006	0.995
1 July '96	0.997	1.017	1.006	1.009

Table C.6-2. The comparison between working standard solution and CSK standard solution at full scale.

Date	Nitrate	Nitrite	Silicate	Phosphate
19 June '96	1.004	0.981	1.025	1.071
21 June '96	1.007	1.004	1.018	1.039
22 June '96	0.994	0.918	1.030	1.027
1 July '96	1.002	0.920	1.018	0.995

The puerility of the nitrite standard solution prepared in this cruise is determined to be 96.6% .

Table C.6-3. The nutrients concentration of LNSW. ($\mu\text{M/l}$)

Batch No.	Station No.	Nitrate	Nitrite	Silicate	Phosphate
3	1-4	0.000	0.000	1.125	0.004
6	5-9	0.000	0.000	1.151	0.000
4	12,13, 18-22	0.000	0.006	1.285	0.018
7	10,11 14-17	0.000	0.003	1.133	0.000
8	23-27	0.000	0.008	1.142	0.028

Table C.6-4 Results of control samples measurement.

	Nitrate	Nitrite	Silicate	Phosphate
Mean ($\mu\text{M/Kg}$)	26.91	0.54	140.63	2.05
STD	0.15	0.01	0.75	0.04
CV(%)	0.55	1.31	0.53	1.81
n	185	185	180	180

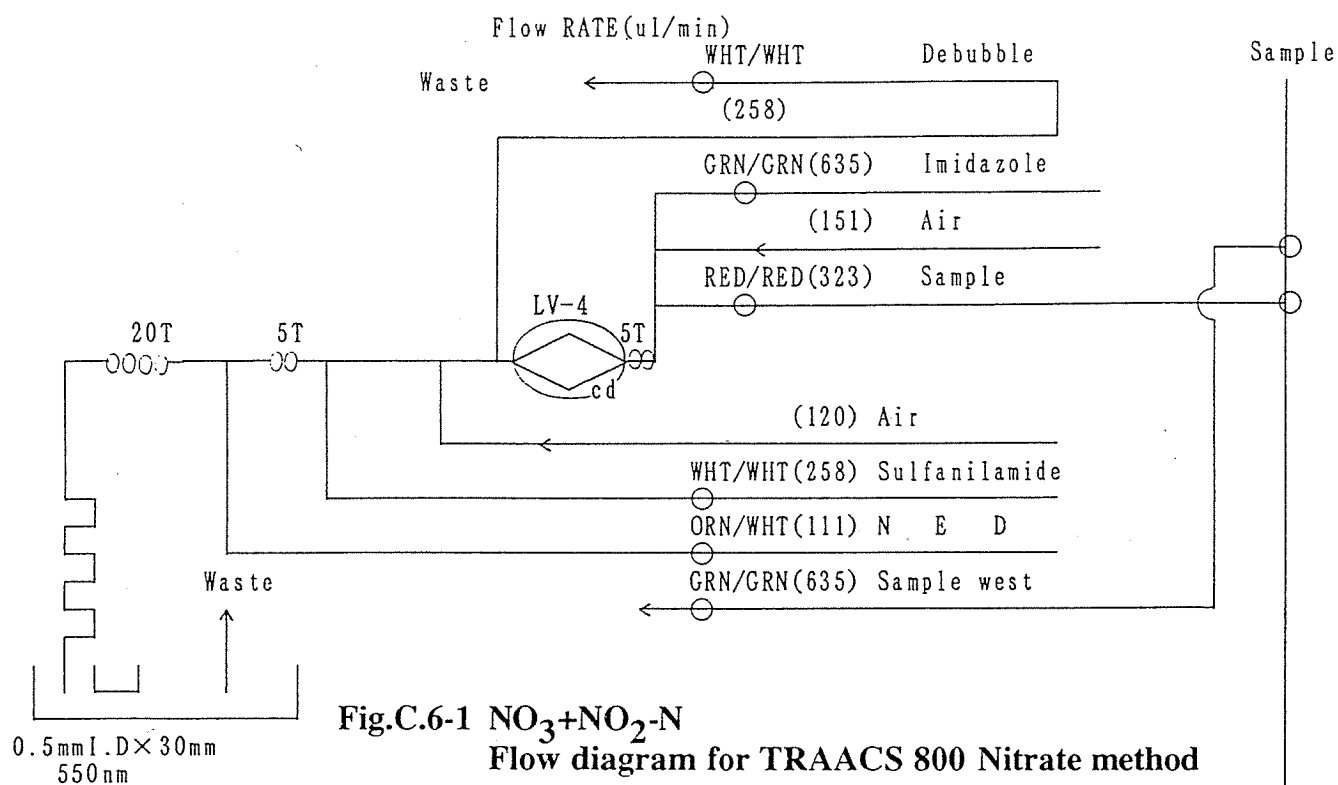
Table C.6-5 Precision at full scale at each analysis.

Station No.	Nitrate CV(%)	Silicate CV(%)	Phosphate CV(%)
1	0.28	0.17	0.60
2	0.41	0.10	0.21
3	0.19	0.26	0.26
4	0.18	0.12	0.32
5	0.19	0.27	0.70
6	0.24	0.18	0.29
7	0.07	0.30	0.53
8	0.18	0.18	0.51
9	0.20	0.22	0.45
10	0.11	0.17	0.46
11	0.13	0.23	0.35
12	0.42	0.21	1.22
13	0.08	0.10	0.26
14	0.12	0.50	0.21
15	0.20	0.11	0.40
16	0.32	0.15	0.21
17	0.26	0.16	0.28
18	0.22	0.17	0.71
19	-	-	-
20	0.28	0.27	0.24
21	0.16	0.36	0.96
22	0.18	0.18	0.92
23	0.18	0.19	0.63
24	0.15	0.25	0.38
25	0.21	0.09	0.61
26	0.28	0.34	0.27
27	0.21	0.10	0.49

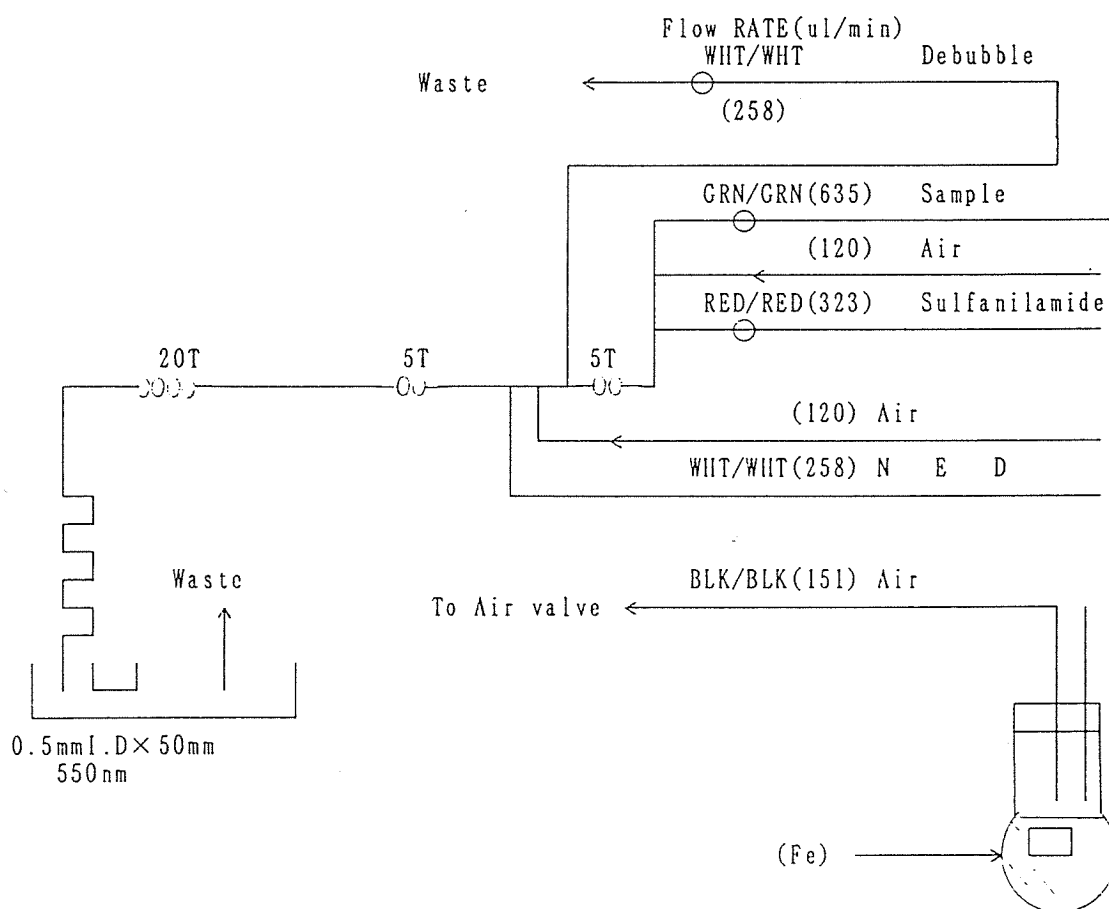
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- Murphy, J., and Riley, J. P., 1962, A modofied single solution method for determination of phosphate in natural water. *Analytica Chimica Acta*, 27, 31-36.

(ch.1)



(ch.2)



Flow diagram for TRAACS 800 Silicate method

Flow RATE (ul/min) WHT/WHT (258) Debubble

Waste

GRN/GRN(635) Molybdate (120) Air

RED/RED(323) Sample

5T H.B. 5T 5T 10T

46°C

(120) Air

WHT/WHT(258) oxalic Acid

ORN/WHT(111) Ascorbic Acid

RED/RED(323) Sample west

Sample

0.5mm I.D x 30mm 630nm

Flow diagram for TRAACS 800 Phosphate method

The diagram illustrates the flow of reagents and samples through a series of valves and a heater block to a waste reservoir. The main flow line starts from a waste reservoir, passes through a 5T valve, a heater block (H.B.) at 46°C, and another 5T valve. This line then splits into several parallel streams: 1) WHT/WHT (258) Debubble, 2) GRN/GRN (635) Sample, 3) (120) Air, 4) RED/RED (323) PO₄ dilute solution, 5) (120) Air, and 6) WHT/WHT (258) Molybdate. All these streams recombine and pass through a third 5T valve before entering a waste reservoir. The waste reservoir is labeled 'Waste' and has an upward arrow indicating flow.

Fig.C.6-4 PO₄-P

C.7 Distribution of oceanic CO₂, pH and TA

by K. Shitashima, D. Tsumune and S. Kraines (September 1996)

1. DESCRIPTION OF METHODS

<pH>

Sea water samples were collected in 100ml polyethylene bottles with inner caps from Niskin-type water samplers. The sample bottles were capped after an overflow of about 100ml sea water. All samples were stored at room temperature after sampling and analyzed within a few hours. Samples were transferred into a closed and jacketed glass measurement cell with a volume of ~30ml. The cell temperature was maintained at a constant temperature of 25C $\pm$ 0.1C. The electric potential and temperature of the sample were measured for 10 minutes with a Ag/AgCl combined electrode (Radiometer Analytical A/S, GK2401C) and a temperature sensor (Radiometer Analytical A/S, T901) connected to a high precision pH meter (Radiometer Analytical A/S, model PHM93). Tris and 2-Aminopyridine Buffers (Dickson and Goyet, 1994) were employed to calibrate pH electrodes. Calibrations were made at the beginning, middle and end of set of measurements for every station.

< Total Alkalinity>

Total Alkalinity samples were collected in 250ml polyethylene bottles with inner caps from Niskin-type water samplers, and capped after an overflow of about 150ml of the sea water. All samples were stored at room temperature after sampling and analyzed within a few hours. Samples were transferred into a glass titration cell using a 50ml transfer pipette and titrated at 25C $\pm$ 0.1C with 0.1 M HCl containing 0.6M NaCl within 10 min. The electric potential and temperature of the sample were followed with a Ag/AgCl combined electrode (Radiometer Analytical A/S, GK2401C) and a temperature sensor (Radiometer Analytical A/S, T901) connected to a TitraLabTM (Radiometer Analytical A/S) system. The titration was controlled automatically and the titration curve was analyzed with the inflection point titration method by the system. The precision of the method was determined to be 0.0043mmol/kg (n=17) from replicate analysis of the Certified Reference Solutions (CRMs (batch 32) supplied by Dr. Andrew Dickson of Scripps Institution of Oceanography (SIO)). Standardization of the titrant (0.1

M HCl) was accomplished with Na₂CO₃ (99.99% pure; Asahi Grass) standards.

<Total dissolved inorganic carbon (T-CO₂)>

The T-CO₂ concentration in seawater samples were determined by using the coulometric titration system (UIC Inc., Carbon Coulometer model 5011) described by Jhonson et al. (1985) with the modified CO₂ extraction system described by Shitashima et al. (1996). A schematic diagram of our system is shown in Fig.C.7-1. Samples for T-CO₂ analysis were drawn from the Niskin samplers into 125ml glass vial bottles after an overflow of about 100ml of the sea water. The samples were immediately poisoned with 50ul of 50% saturated HgCl₂ in order to restrict biological alteration prior to sealing the bottles. All samples were stored in a refrigerator before measurement, and were analyzed within 12 hours of collection.

Seawater was introduced manually into the thermostated (25C $\pm$ 0.1C) measuring pipette with a volume of ~30ml by a pressurized headspace CO₂-free air that had been passed through the KOH scrubber. The measured volume was then transferred to the extraction vessel. The seawater sample in the extraction vessel was acidified with 1.5 ml of 3.8% phosphoric acid and the CO₂ was extracted from the sample for 10 minutes by bubbling with the CO₂-free air. After passing through the Ag₂SO₄ scrubber and polywool to remove sea salts and water vapor, the evolved CO₂ gas was continuously induced to the coulometric titration cell by the stream of the CO₂-free air. All reagents were renewed every day.

The T-CO₂ concentration in seawater was calculated using a calibration curve constructed by measuring five to six different concentration of dissolved Na₂CO₃ (99.99% pure; Asahi Grass) used as a standard solution (Dickson and Goyet, 1994). The precision of the T-CO₂ measurements was tested by analyzing CRMs (batch 32) at the start of the measurement of samples every day. Fig.C.7-2 shows a comparison between the results of our shipboard measurements of these CRMs during the cruise and certified values provided by Dr. Andrew Dickson. Our shipboard measurements yielded a mean value of 1995.6 $\pm$ 2.8 μ mol/kg (n=40), which compares with 1997.6 $\pm$ 1.4 μ mol/kg (n=9) certified by SIO. We also prepared and analyzed sub-standards that were bottled into 125ml glass vial bottles from a 20l bottle of filtered and poisoned offshore surface water in order

to check the condition of the system and the stability of measurements every day. The resulting standard deviation from replicate analysis of 19 sub-standards was ± 1.8 $\mu\text{mol/kg}$.

2. PRELIMINARY RESULTS

Fig.C.7-3 shows the vertical distributions of pH, Total-Alkalinity and T-CO₂ concentration at 1 degree intervals between 10N and 1N along 130E. The fluctuation of the vertical distributions of Total-Alkalinity at some of the stations was caused by electrical problems with the onboard measurement. The T-CO₂ maximum layer at each station gradually deepened towards the north. This trend suggests that this layer represents the northward flowing of the Philippine Sea bottom water.

3. REFERENCES

- Dickson, A. G. and C. Goyet. 1994. Handbook of methods for the analysis of the various parameters of the carbon dioxide system in sea water. Ver. 2 ORNL/CDIAC-74. A. G. Dickson and C. Goyet (eds.). Carbon Dioxide Information Analysis Center, Oak Ridge National Laboratory, Oak Ridge, Tenn.
- Jhonson, K. M., A. E. King, and J. M. Sieburth. 1985. Coulometric TCO₂ analysis for marine studies: An introduction. Mar. Chem. 16, 61-82pp
- Shitashima, K., K. B. Steven, D. Tsumune, I. Asamuma, and T. Ono. 1996. The measurement of total carbonate in seawater.: In abstract of the 1996 spring meeting of the Oceanographic Society of Japan. 269pp (in Japanese)

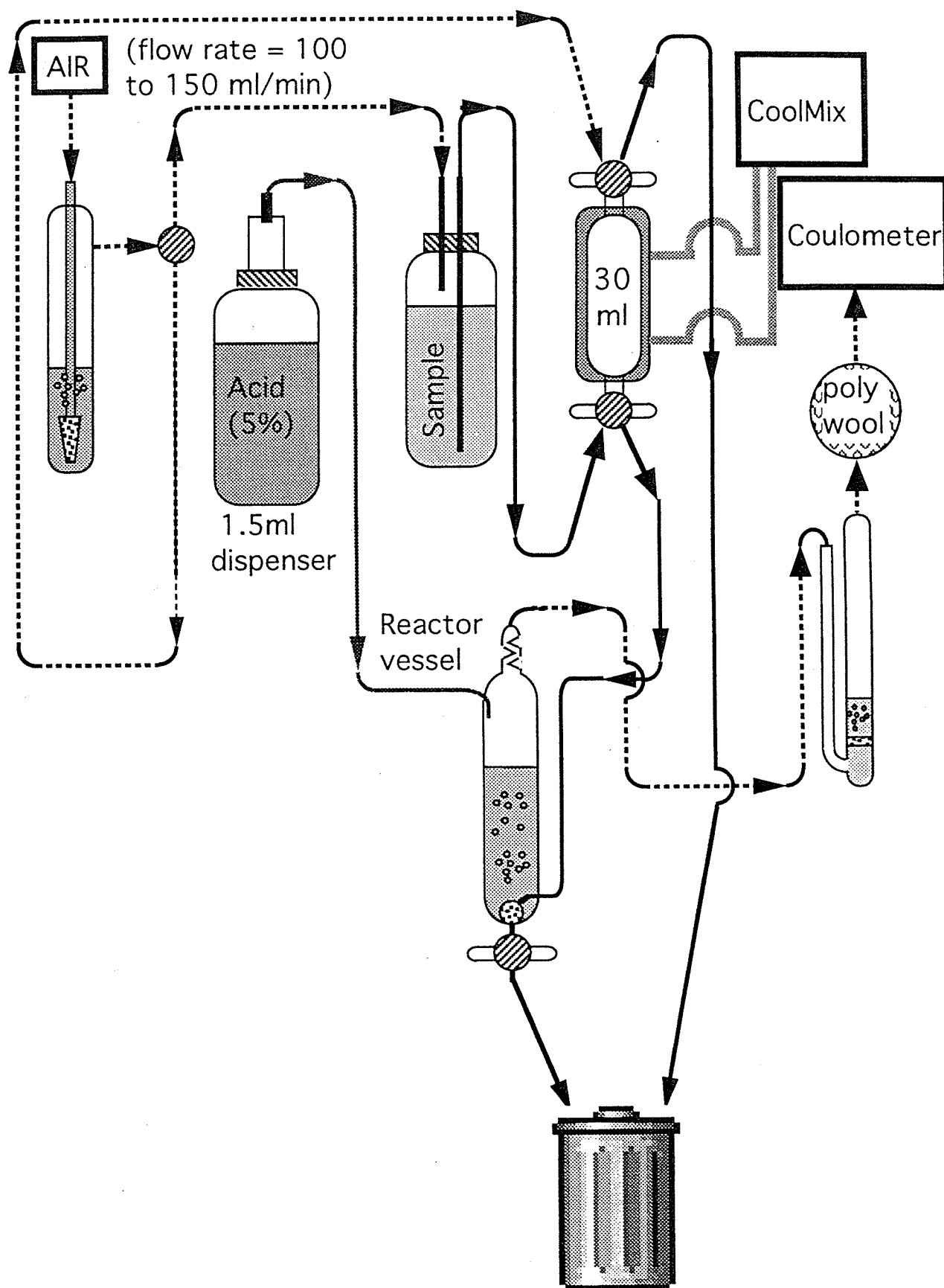


Fig. C.7-1 The schema of modified T-CO₂ analysis system

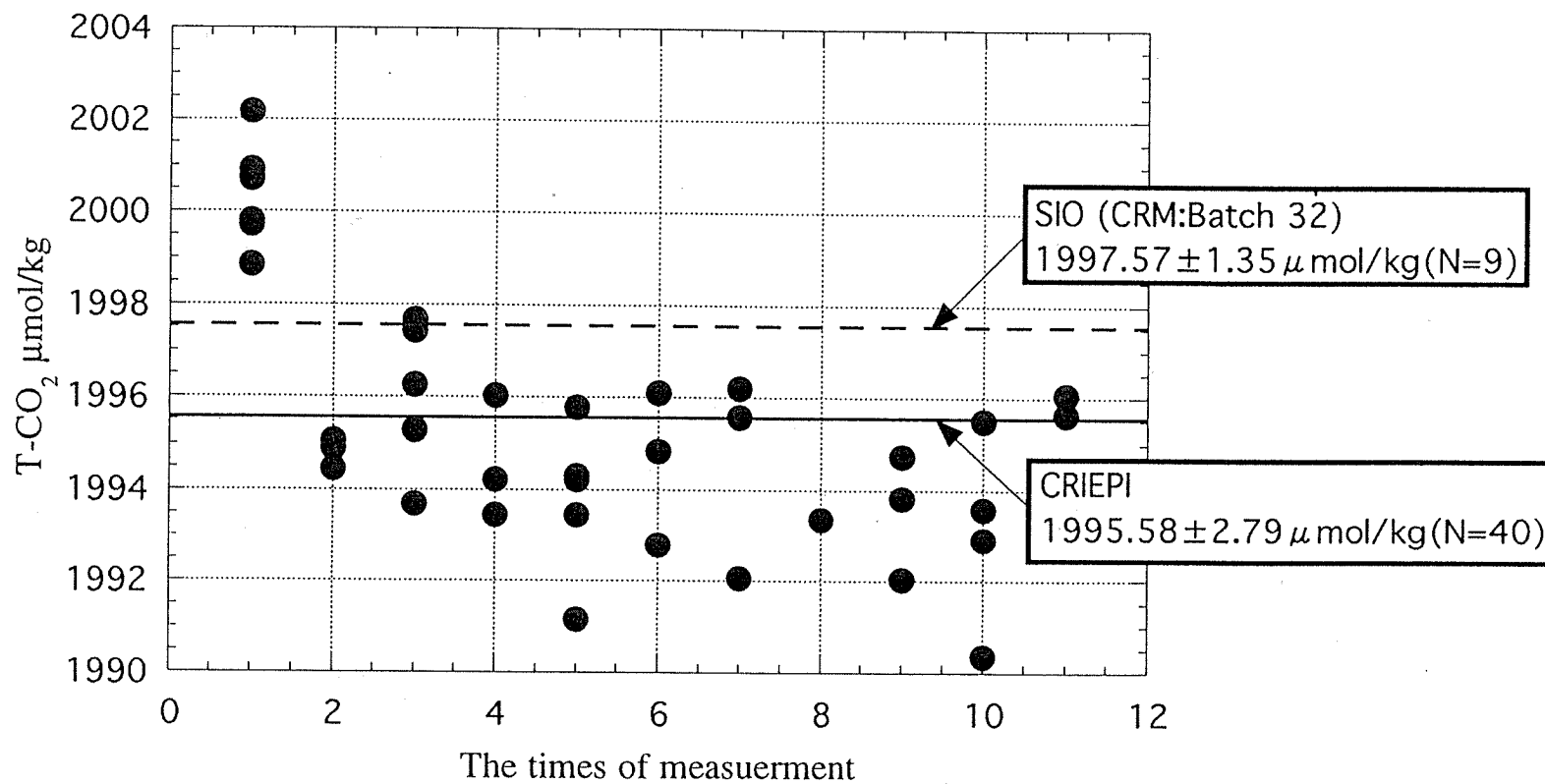


Fig. C.7-2 Comparison between the results of our shipboard measurements of these CRMs during the cruise

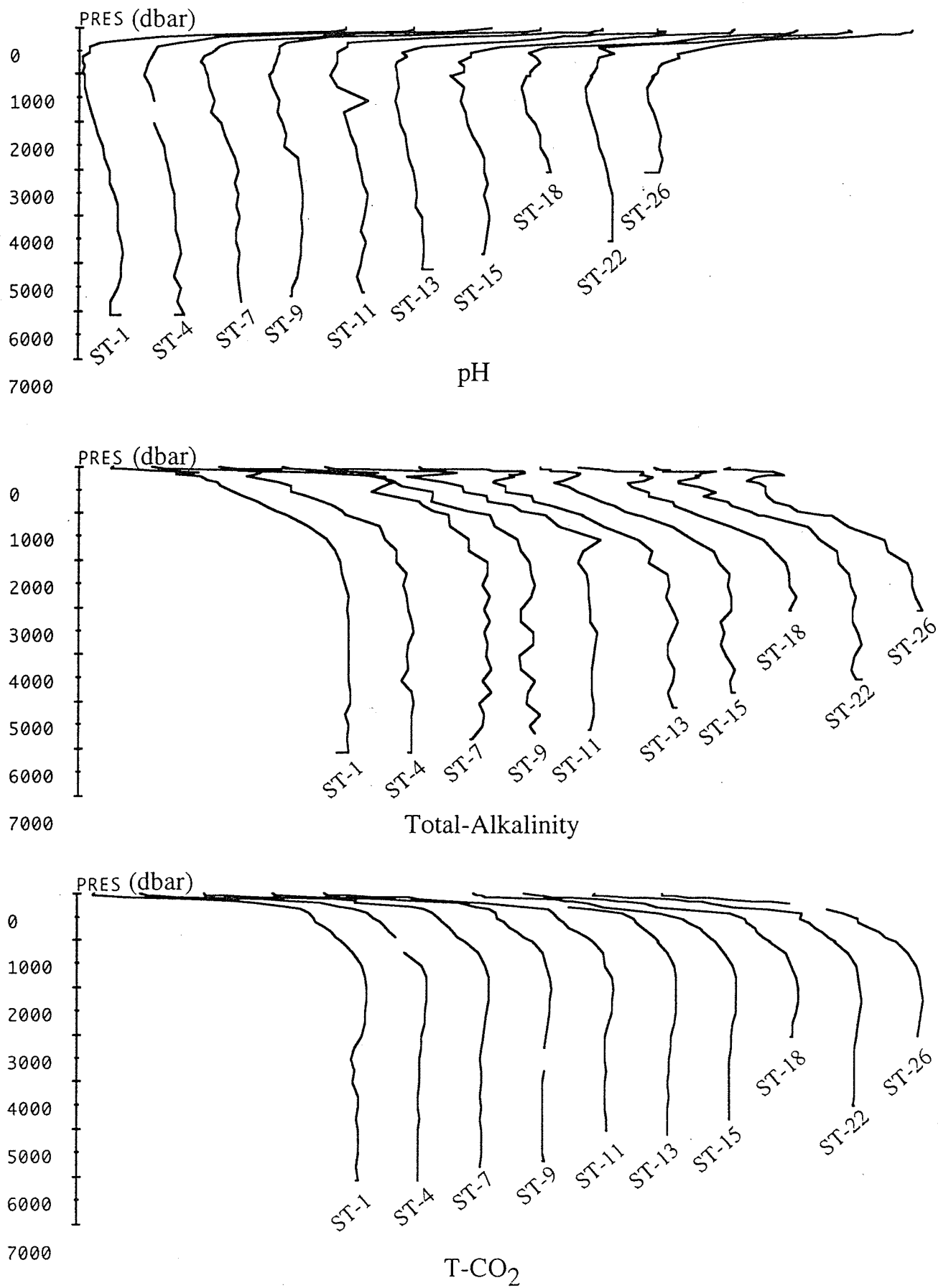


Fig. C.7-3 Vertical distributions of pH, Total-Alkalinity ($\mu\text{mol/kg}$) and T-CO₂ ($\mu\text{mol/kg}$)

C.8 Tracers

by C. Saito and N. Harada (6 September 1996)

C-14

All samples were drawn from 12 liter Niskin bottles followed that for oxygen or TCO₂. Samples were drawn into glass vials of ca. 200 ml. These were rinsed before filling and overflowed by two to three times of the vial volume. Then 50 mg of saturated HgCl₂ solution was added and subsequently rubber cap and aluminum cap were clamped to vials.

Duplicate samples were drawn from the same rosette bottle at all sampling depths. Sampling stations were 1, 4, 7, 9, 11, 13, 15, 18, 22 and 26. The sampling depths of radiocarbon samples shallower than 1000 meters were 30, 50, 100, 200, 300, 400, 500, 800, 1000. Below 1000 meters the sampling interval was 500 meters.

Helium

Samples were transferred the first from Niskin bottle to the copper tube using a gravity feed technique through lengths of plastic tubing. We followed helium sampling procedure by WOCE manual (Jenkins et al., 1991). The seal was made by crimped to form a pressure welded seal. Helium sampling stations were same as radiocarbon sampling site but those layers were very few.

Tritium

Sampling bottles for tritium were baked for a few hours at about 180 C. The inside of this bottle was sealed with argon gas. Sea water sample was introduced into the bottle with a plastic tubing. The bottle was filled within a few centimeters of the top and head space was retained. The cap of ground joint glass bottle was immediately replaced and taped. Tritium sampling stations and depths were same as radiocarbon sampling.

References

Jenkins, W. J., D. E. Lott, M. W. Davis, S. P. Birdwhistell and M. O.

Matthewson 1991. Measuring helium isotopes and tritium in seawater samples. WHP Office Report WHPO 91-1, Woods Hole, Mass., USA.

C.9 Weather and sea condition

by S.Ishida(Captain of R/V KAIYO) and N.Yoshioka (September 1996)

Weather condition was very good through our cruise, as it was covered by the North Pacific high pressure, Any typhoon nor developing low pressure were not appeared around eastern part of the tropical Pacific area on the duration of our cruise. Accordingly, any strong swell nor waves did not disturb our CTD and Rosetta casting operations.

C.10 Problems

by Y.Kashino (2 December, 1996)

As described in A.5, the damage on a fiber of armored-wire of CTD cable occurred during this cruise. Because of this accident, we must slow CTD decent rate at irregular winding after st.12. This effected not only the time schedule but also the quality of CTD data because of increase of shed wakes. The rate of bad data detected changed from 8.8% to 11.1 % before and after this accident.

D. Acknowledgements

by N.Yoshioka (September 1996)

We would like to great acknowledge for contribution of many scientist and technicians, who joined to this cruise from their institution or company. We also would like to greatly thanks for helpful supports by the captain Ishida and the crew on R/V KAIYO. Technics for water sampling, chemical analysis and CTD data processing were totally taken over from previous KAIYO cruises (WOCE-PR1S and PR24 in 1994, PR23 and PR24N in 1995). We would like to great thanks to Mr.Michio Aoyama and Mr.Takeshi Kawano who developed these techniques and constructed the accuracy control system on R/V KAIYO.

The WOCE cruise and publication of this data report were all supported by Tropical Ocean Climate Study (TOCS) conducted by the JAMSTEC, which has been funded by the Science and Technology Agency (STA), JAPAN.

E. References

see each section

F. Appendices

F.1. Section plot along P8S.

Figure F.1-1. Temperature (CTD)

Figure F.1-2. Salinity (CTD)

Figure F.1-3. Dissolved oxygen (sampled water)

Figure F.1-4. Silicate (sampled water)

Figure F.1-5. Nitrate (sampled water)

Figure F.1-6. Phosphate (sampled water)

Figure F.1-7. Total Carbon (sampled water)

Figure F.1-8. pH (sampled water)

Figure F.1-9. Zonal velocity in m/sec (ADCP).

Solid contour denote eastward flow.

Figure F.1-10. Meridional velocity in m/sec (ADCP).

Solid contour denote northward flow.

F.2 Velocity vectors measured by ADCP.

Figure F.2-1. On the depth of 50m

Figure F.2-2. On the depth of 100m

Figure F.2-3. On the depth of 150m

Figure F.2-4. On the depth of 200m

Figure F.2-5. On the depth of 250m

Figure F.2-6. On the depth of 300m

Figure F.2-7. On the depth of 350m

Figure F.2-8. On the depth of 400m

Figure F.2-9. On the depth of 450m

Figure F.2-10. On the depth of 500m

Temperature

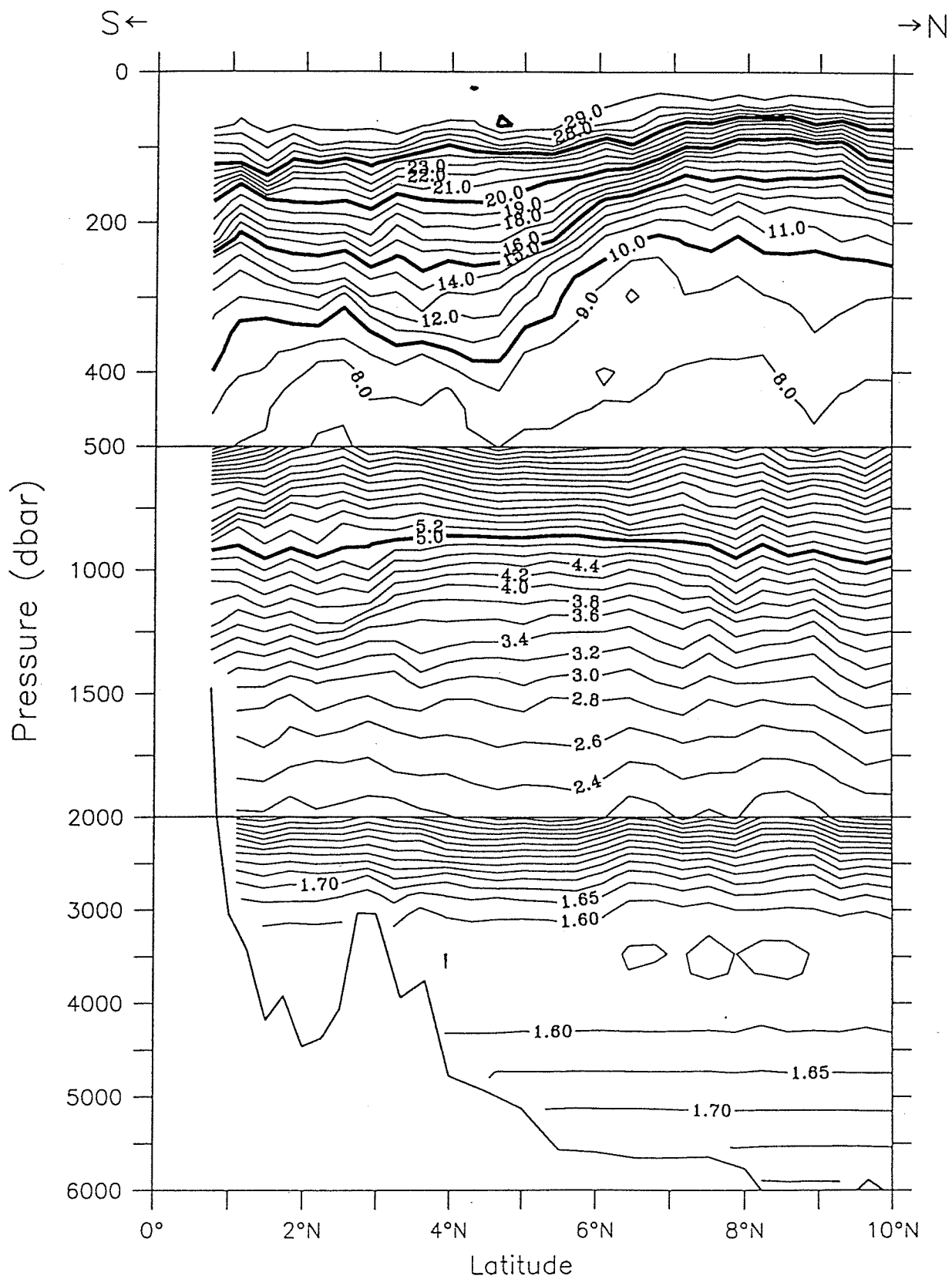


Figure F.1-1. WOCE96 P8S

Salinity

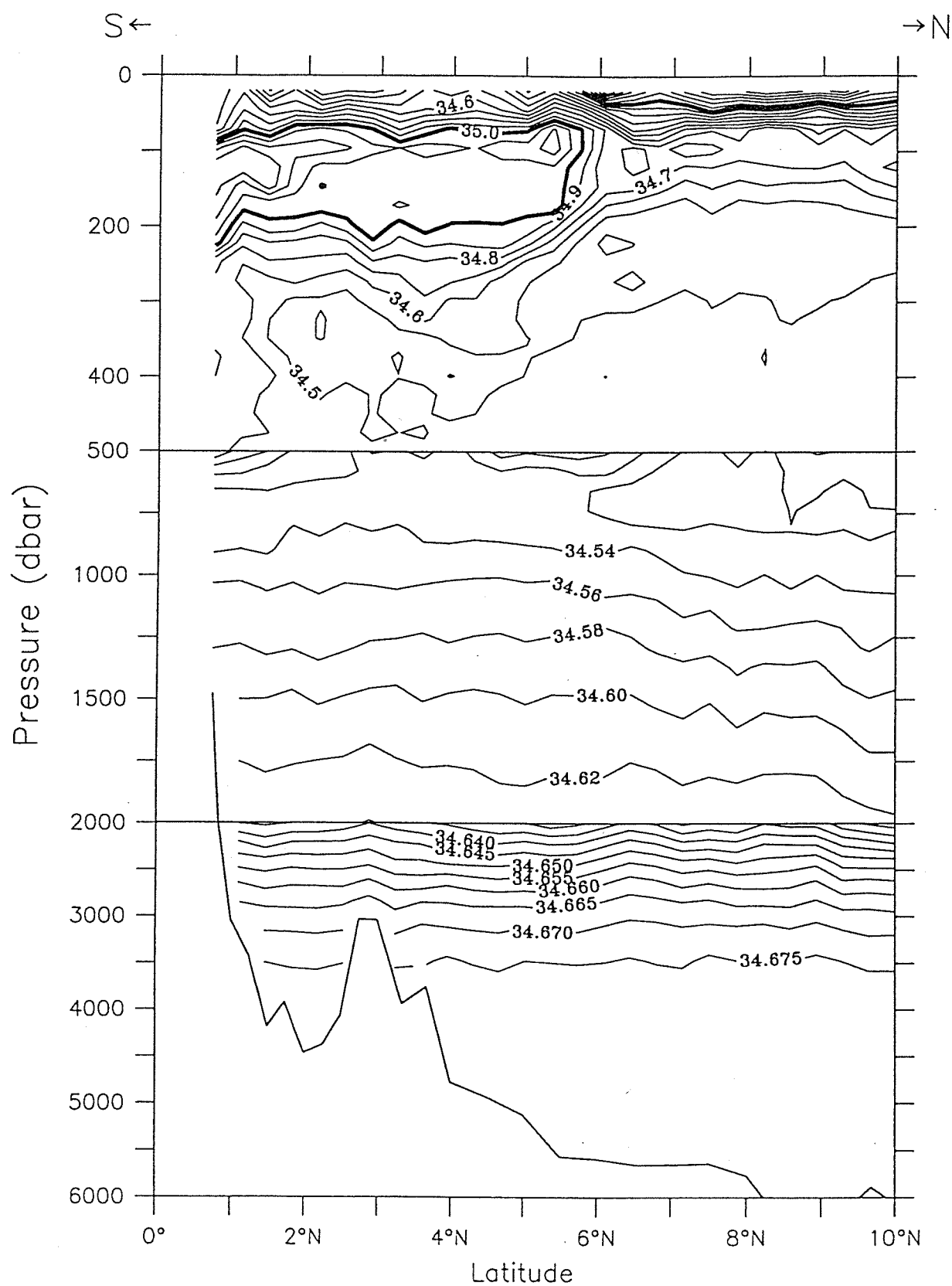


Figure F.1-2. WOCE96 P8S

Oxygen ($\mu\text{mol/kg}$)

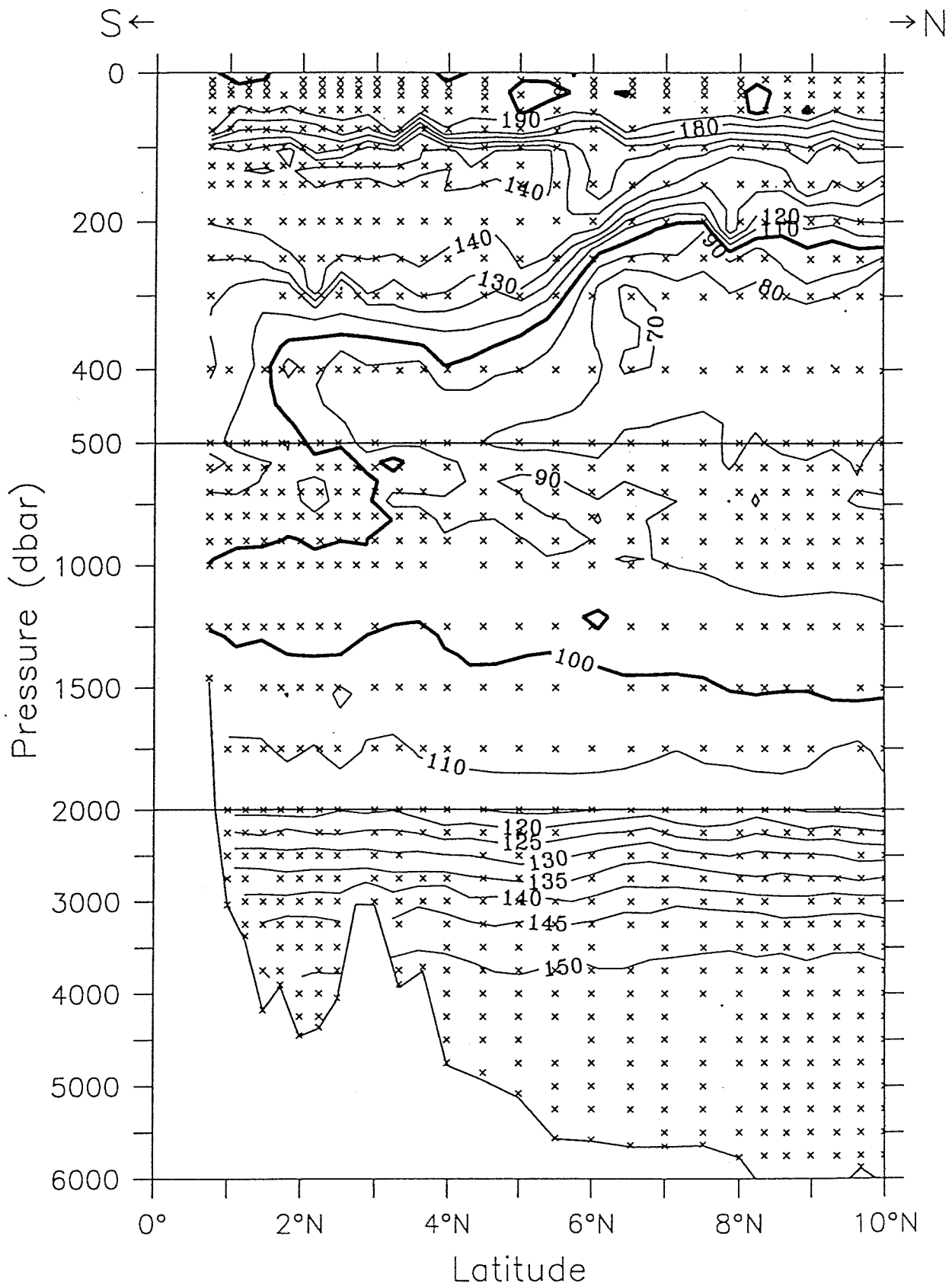


Figure F.1-3. WOCE96 P8S

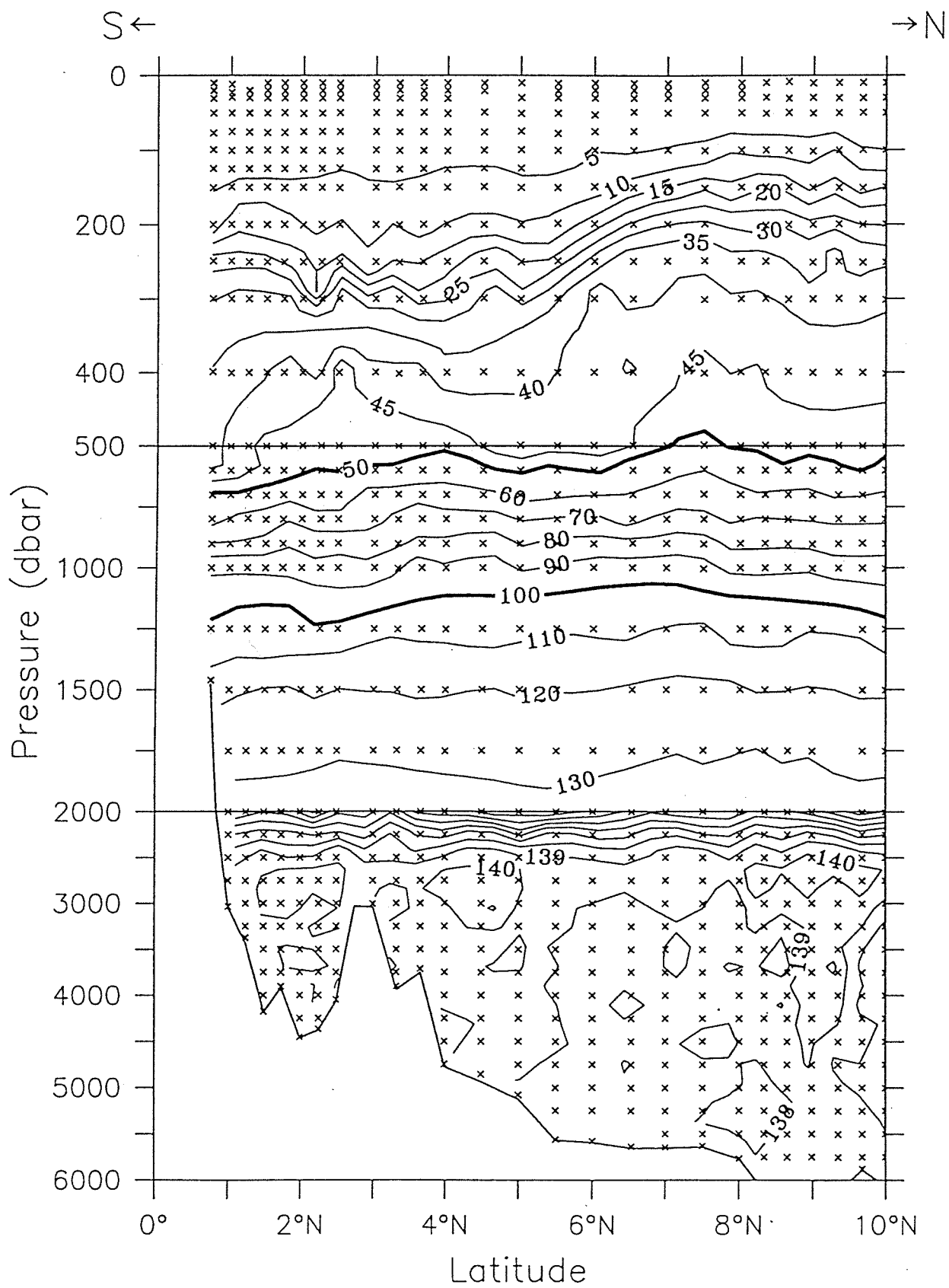
Silicate ($\mu\text{mol/kg}$)

Figure F.1-4. WOCE96 P8S

Nitrate ($\mu\text{mol/kg}$)

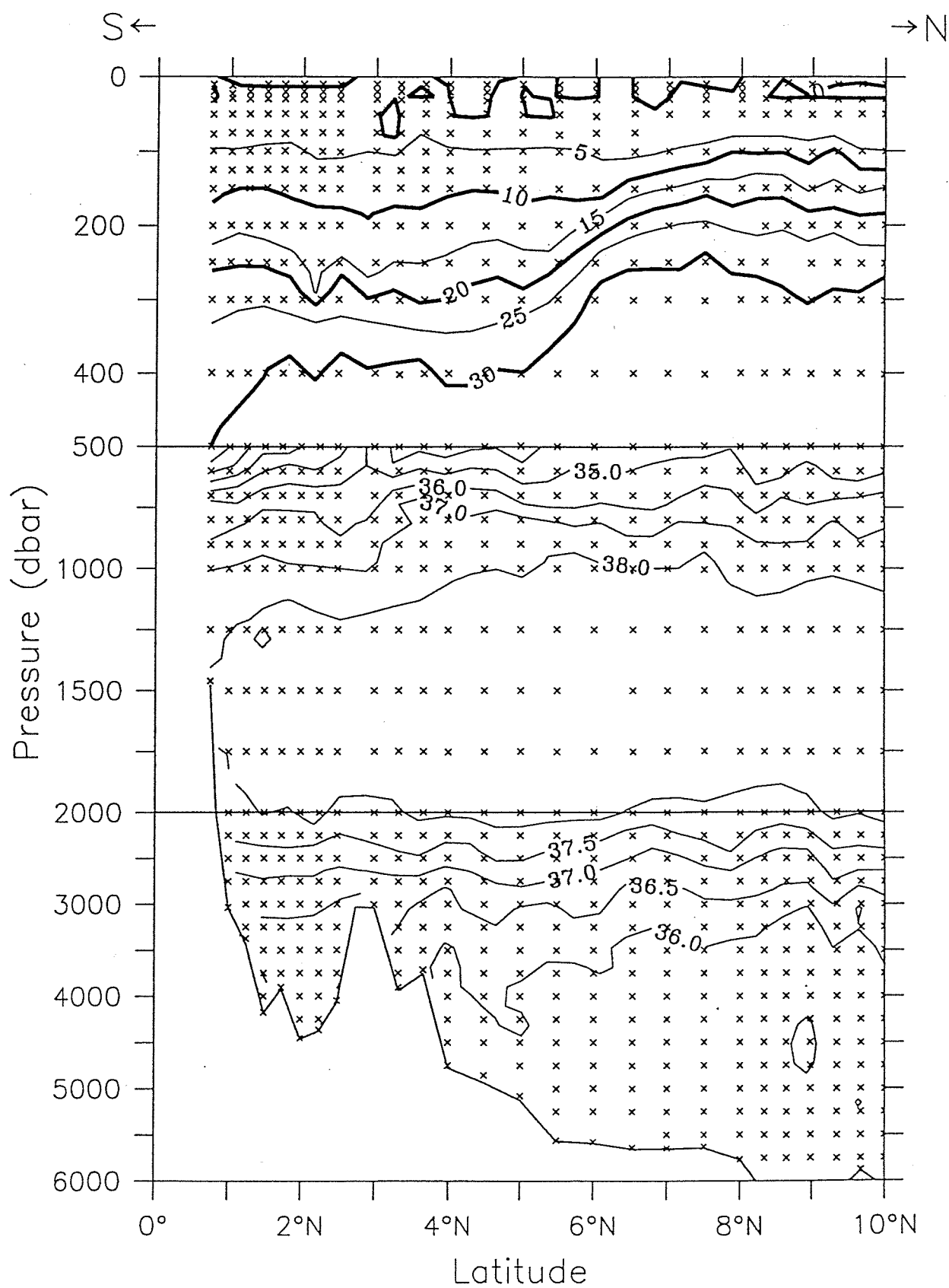


Figure F.1-5. WOCE96 P8S

- 60 -

Total Carbon ($\mu\text{mol/kg}$)

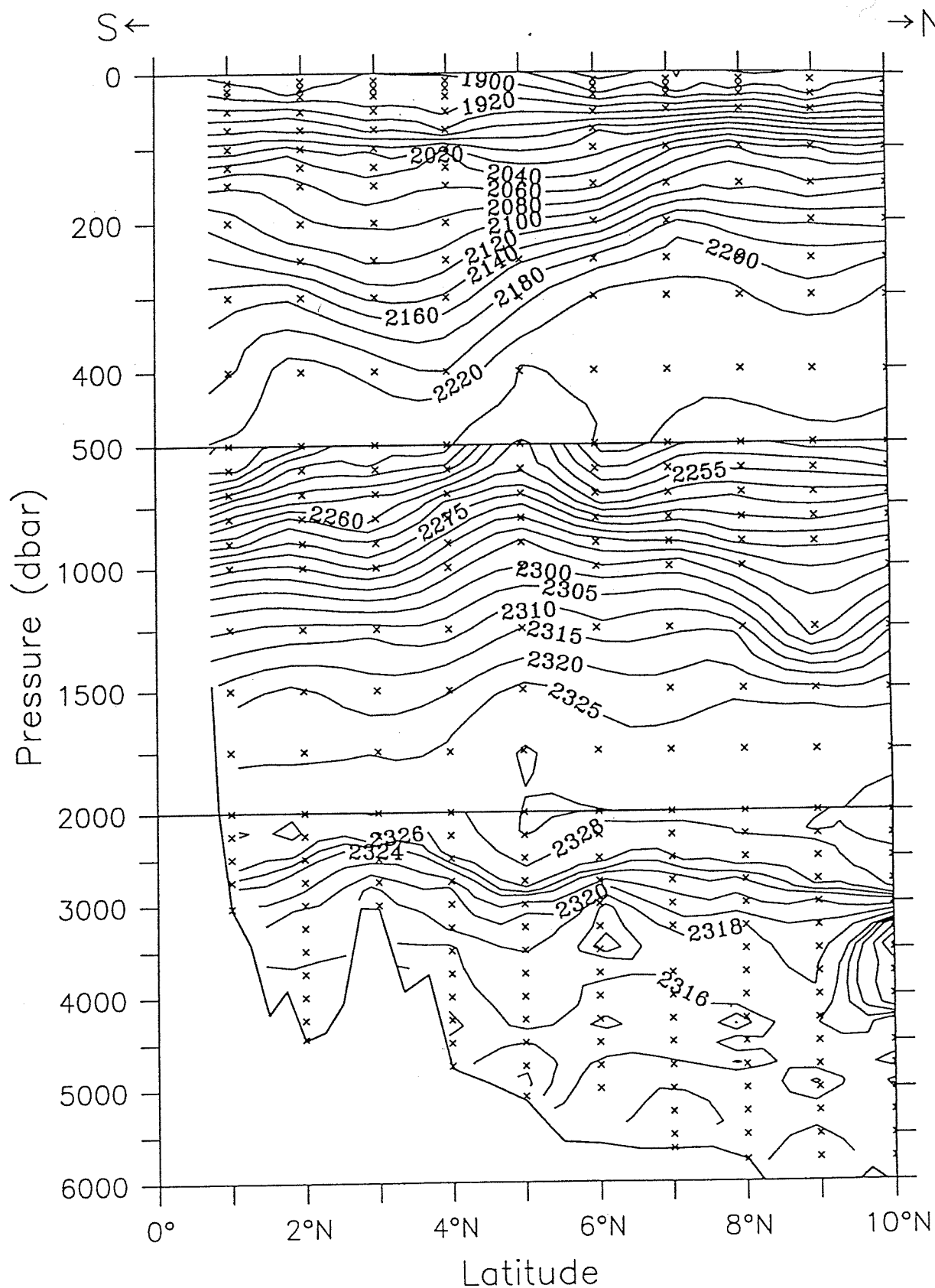
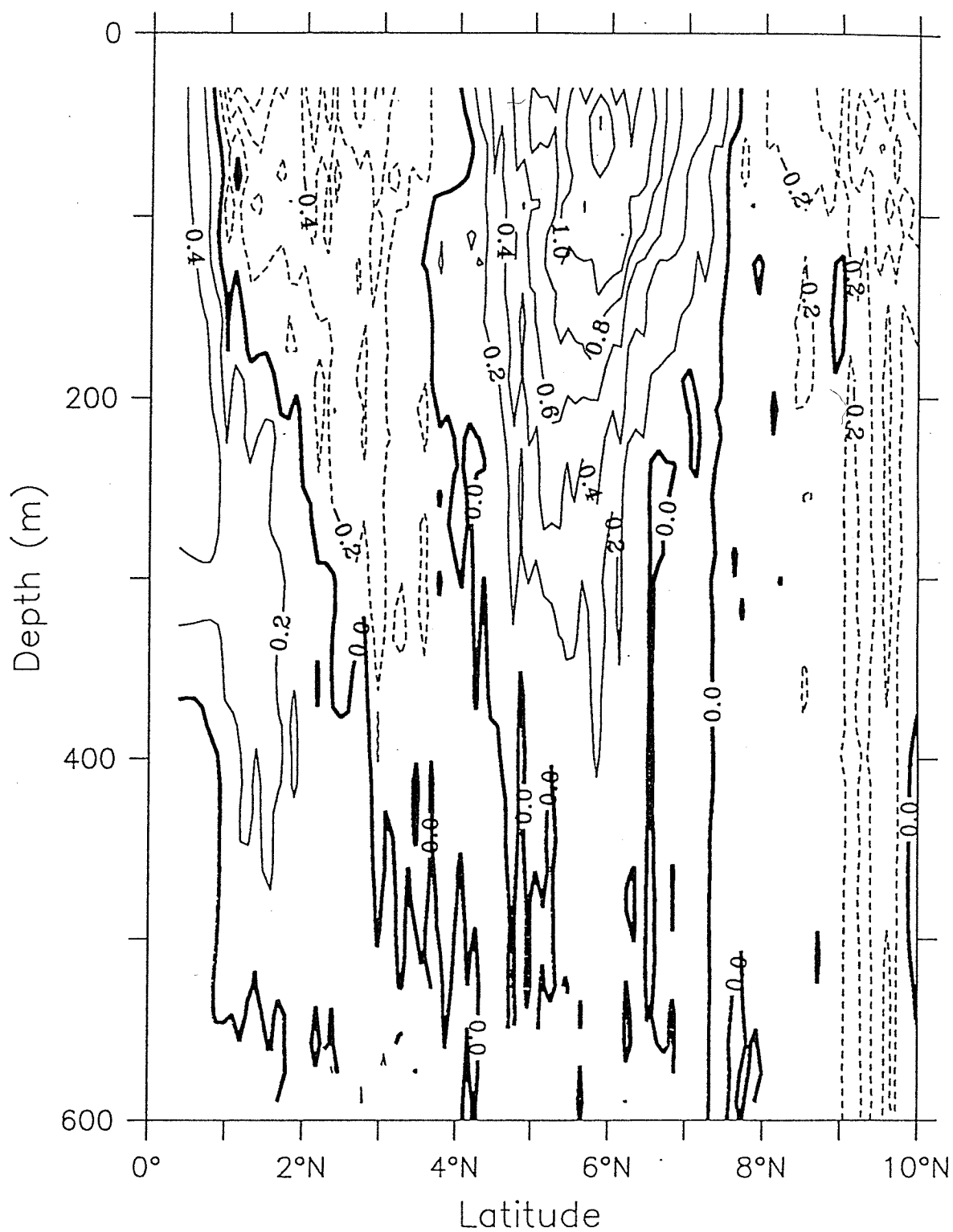


Figure F.1-7. WOCE96 P8S

Figure F.1-8.

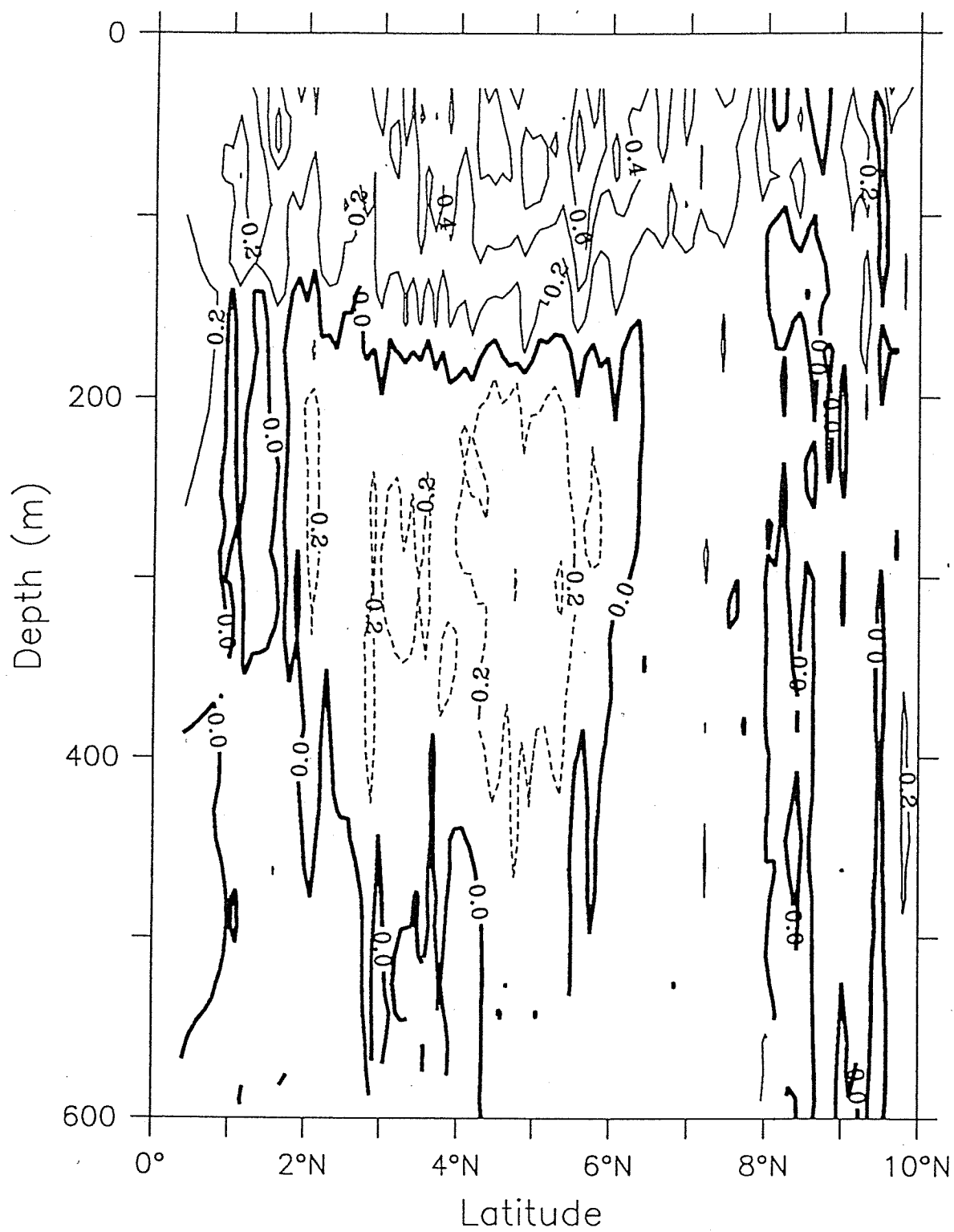
ADCP Velocity (E-W)



WOCE96 P8S

Figure F.1-9.

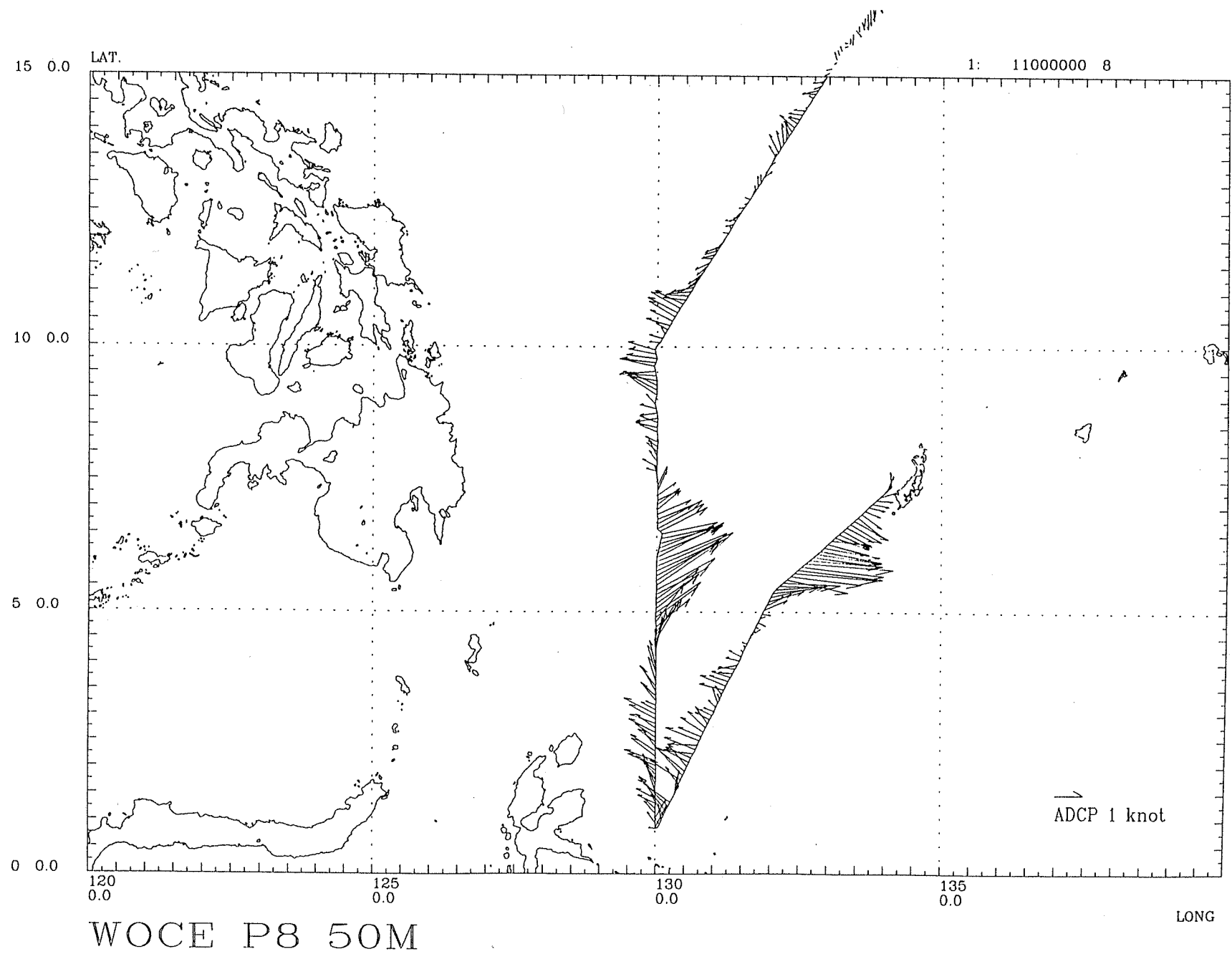
ADCP Velocity (N-S)



WOCE96 P8S

Figure F.1-10.

Figure F.2-1.



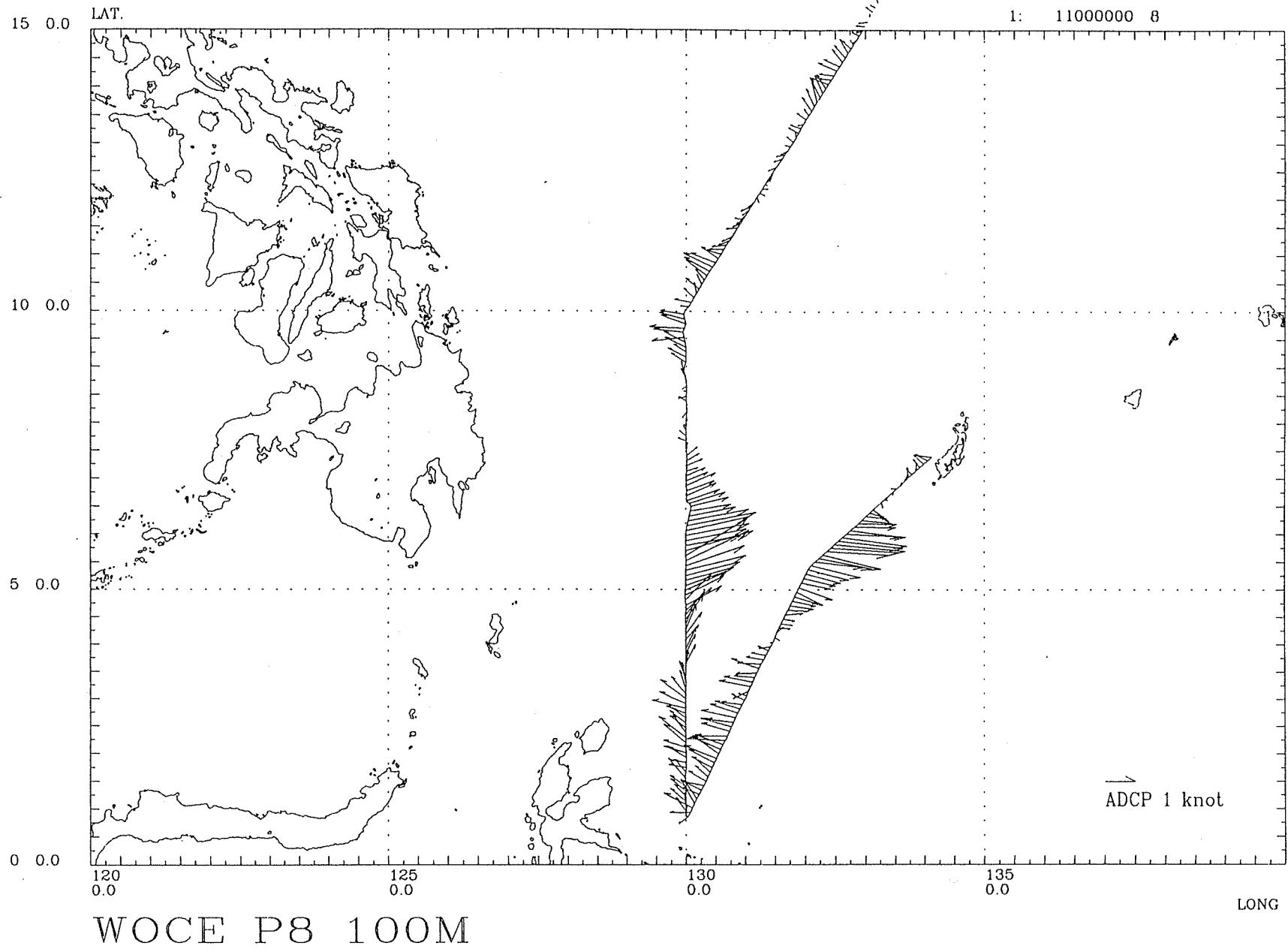
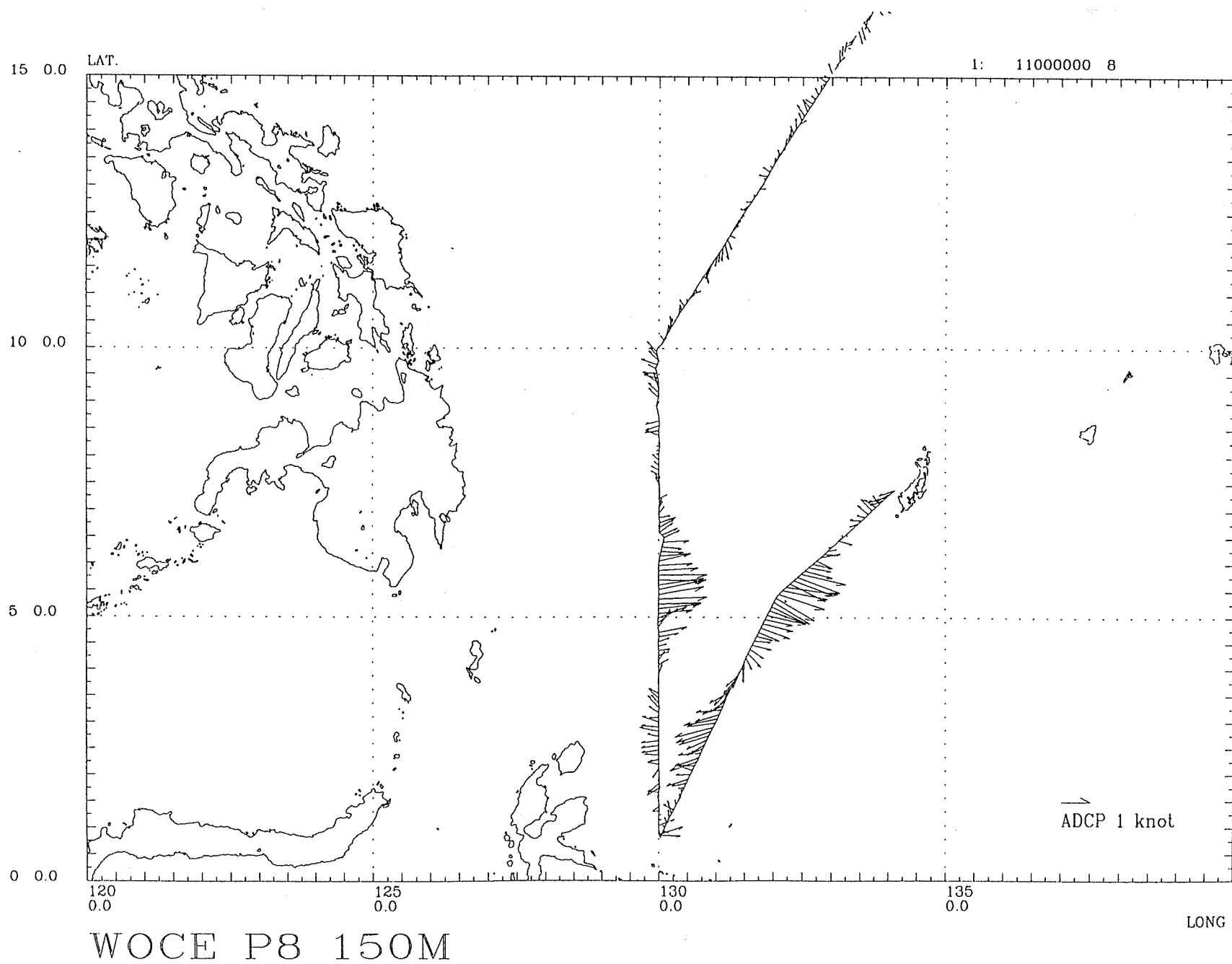


Figure F.2-2.

Figure F.2-3.



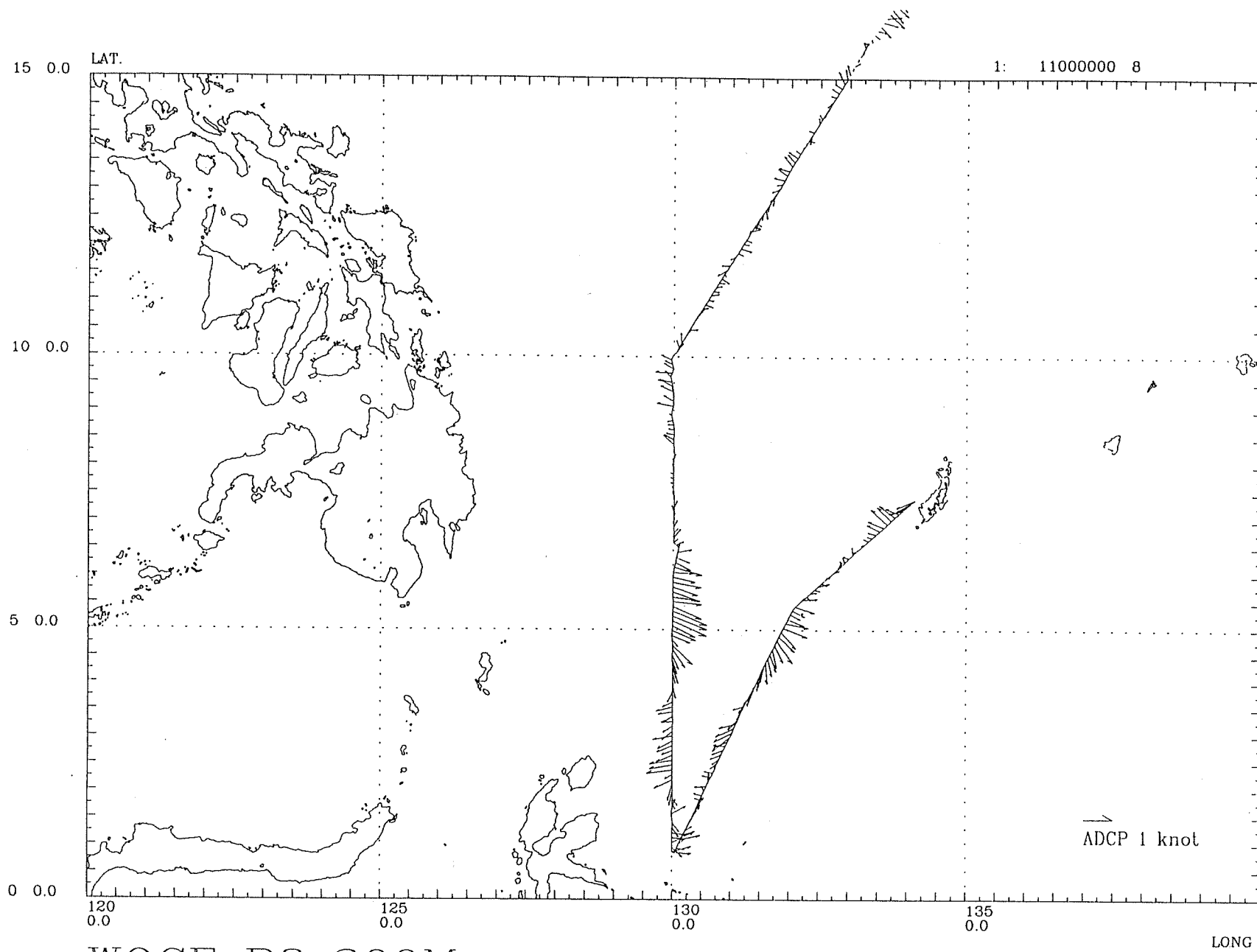
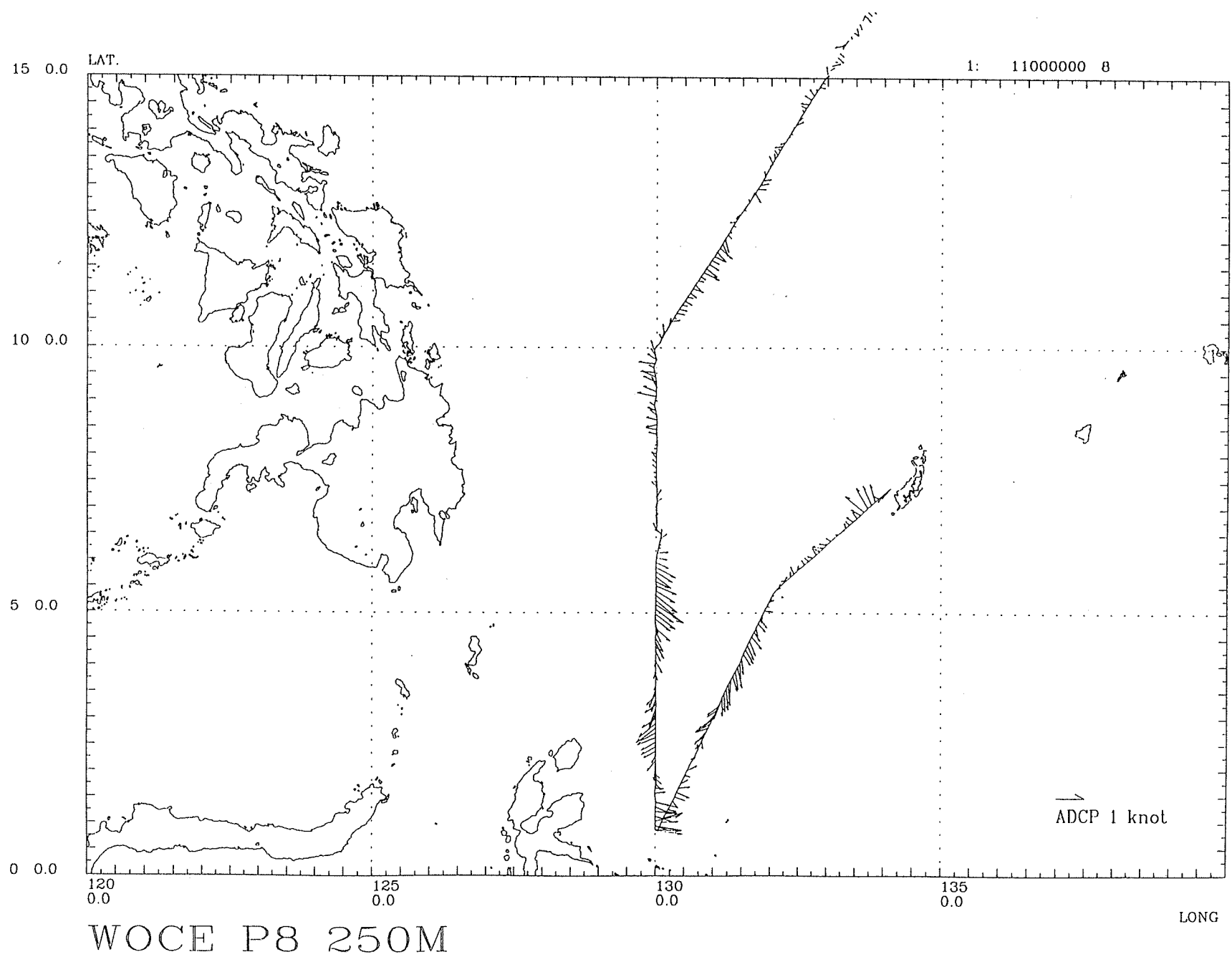


Figure F.2-4.

Figure F.2-5.



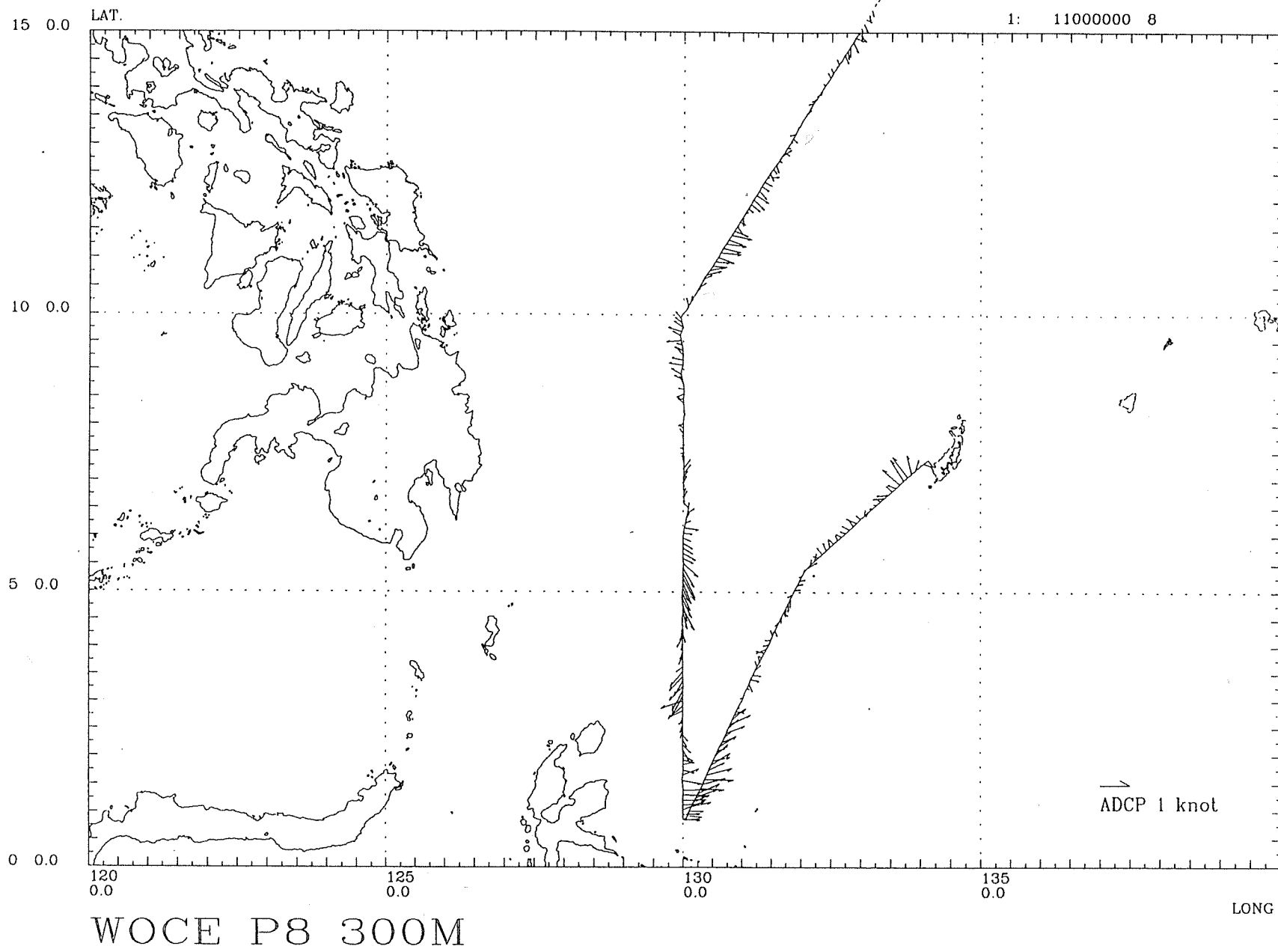


Figure F.2-6.

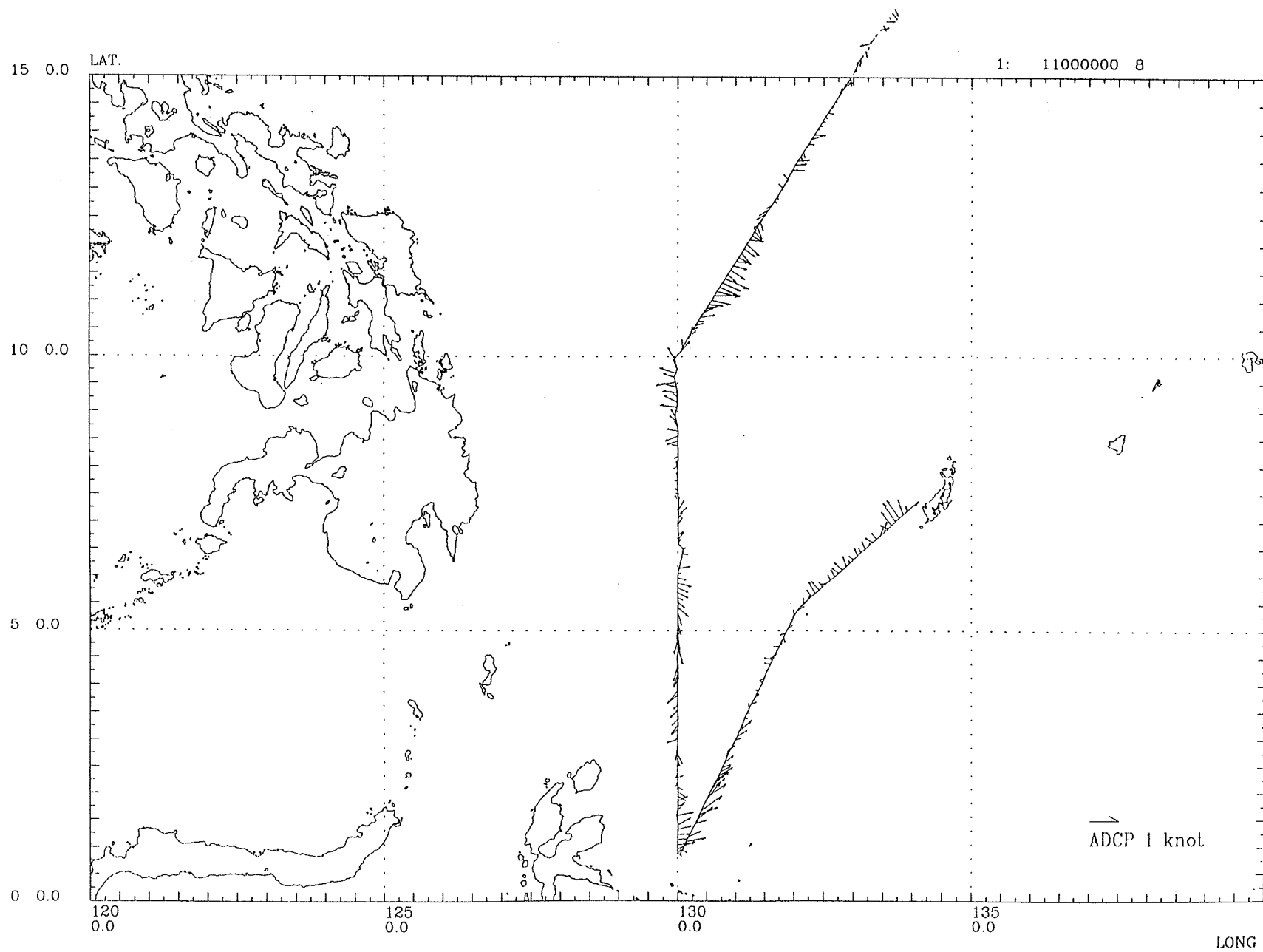


Figure F.2-7.

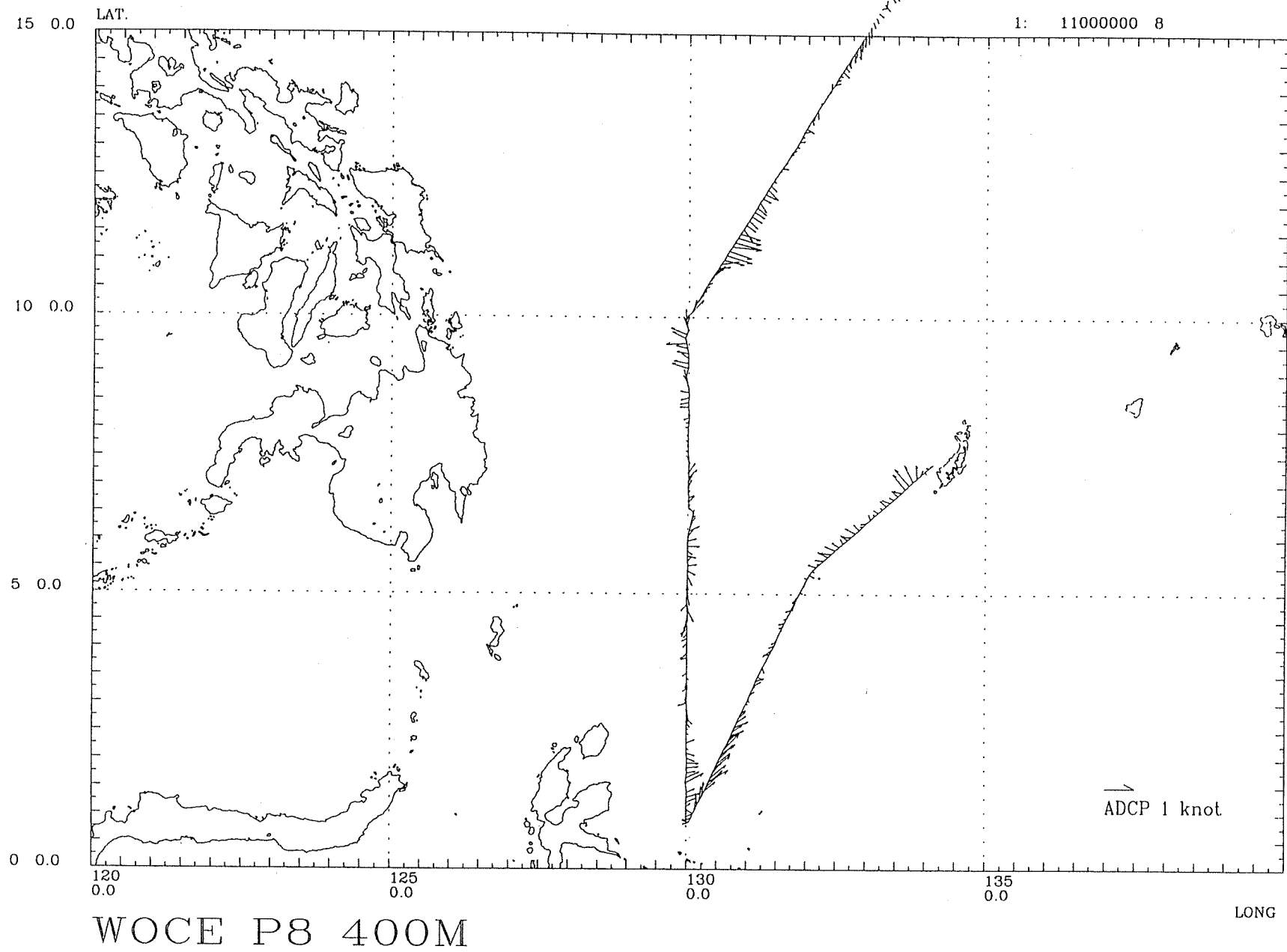


Figure F.2-8.

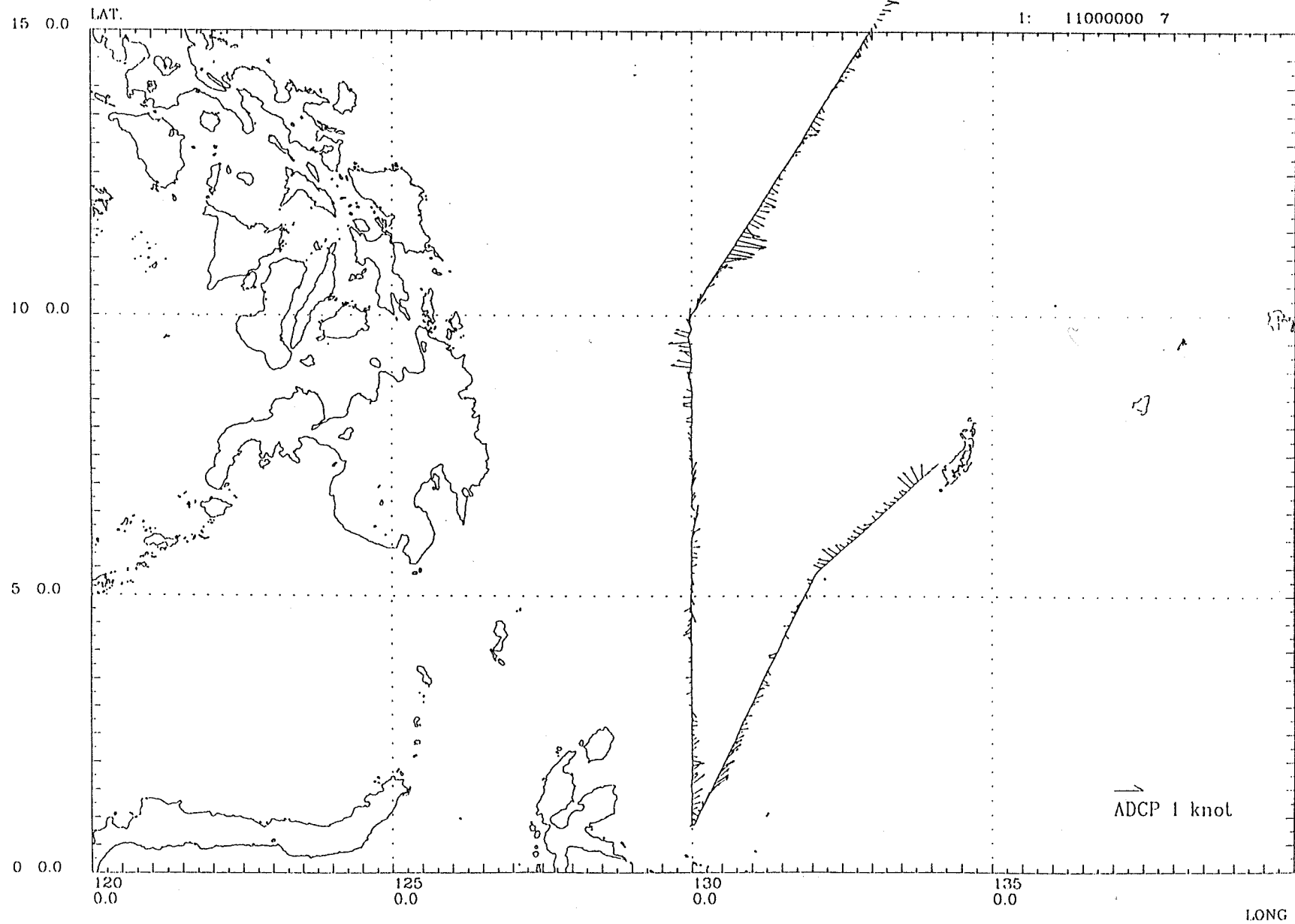


Figure F.2-9.

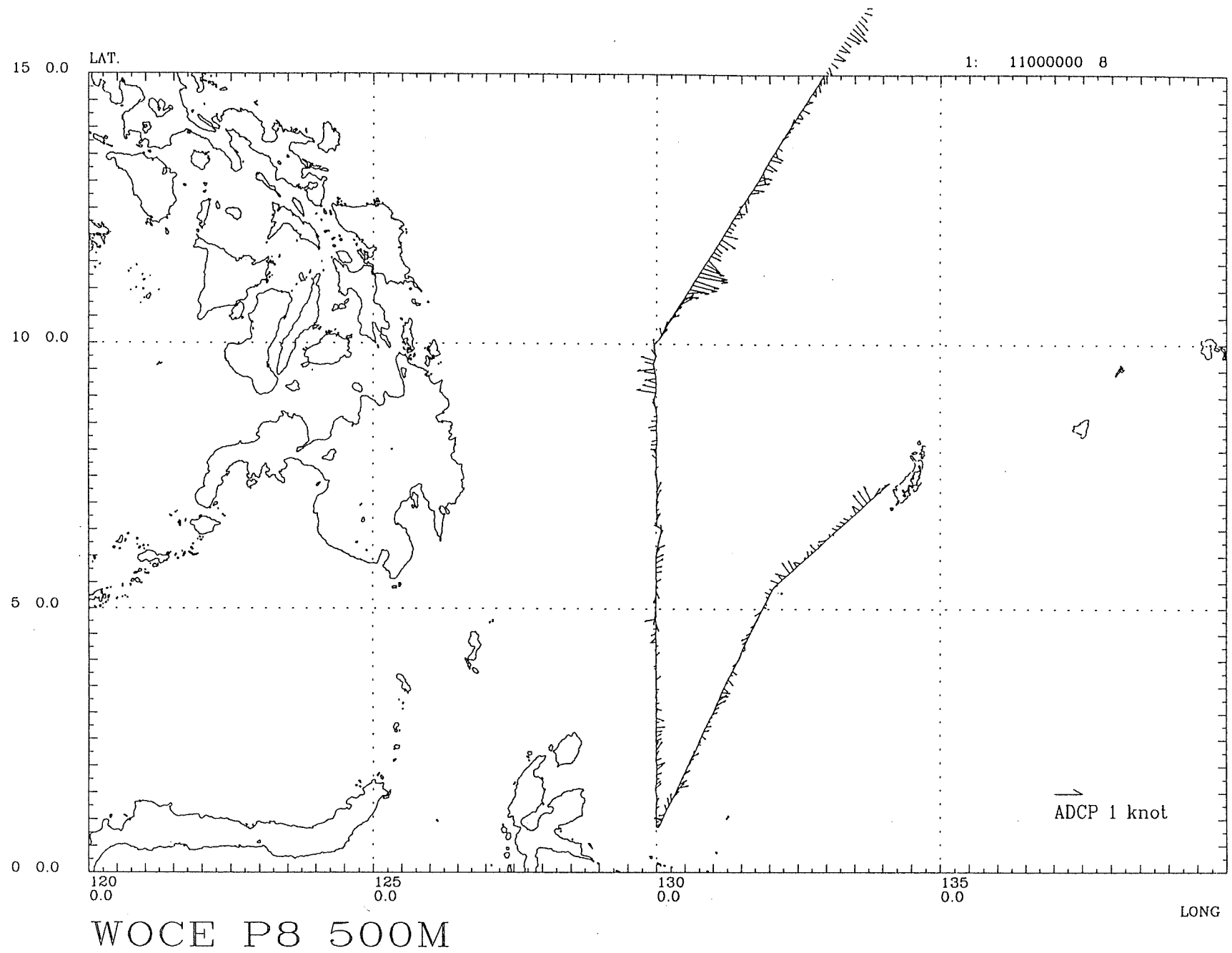


Figure F.2-10.

R/V KAIYO(Country code 49,ship code is XK) Expedition designation-cruise number XK9605 along WHP section southern part of P8

EXPOCODE	WHP-ID	STNNBR	NO	TYPE	DATE	TIME	CODE	POSITION	CODE	UBD	HBD	MW	MAXP	NOB	PARAMETER	COMMENT
49XK9605	P8S	01	1	ROS	062396	0342	BE	10 00.04 N 129 59.85 E	GPS	5920						
49XK9605	P8S	01	1	ROS	062396	0518	BO	09 59.77 N 129 58.72 E	GPS	5913	13	6129	6054	36	1-6,9,10,12,23,24,26	
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49XK9605	P8S	02	1	ROS	062396	1230	BO	09 40.80 N 129 58.41 E	GPS	5761	15	6267	5873	36	1-6	
49XK9605	P8S	02	1	ROS	062396	1455	EN	09 41.87 N 129 56.99 E	GPS	5728						
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49XK9605	P8S	03	1	ROS	062396	2137	EN	09 21.07 N 130 00.06 E	GPS	5930						
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49XK9605	P8S	04	1	ROS	062496	0110	BO	08 59.25 N 129 58.19 E	GPS	5865	11	6172	6035	36	1-6,9,10,12,23,24,26	
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49XK9605	P8S	13	1	ROS	062696	1427	BO	05 00.08 N 129 59.44 E	GPS	5038	48	5036	5079	35	1-6,9,10,12,23,24,26	
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49XK9605	P8S	14	1	ROS	062696	2030	BE	04 30.02 N 130 00.27 E	GPS	4833						

49XK9605	P8S	14	1 ROS 062696 2159 B0	04 30.03 N 129 59.93 E GPS	4845	82	4753	4856	36	1-6
49XK9605	P8S	14	1 ROS 062796 0110 EN	04 29.60 N 129 58.97 E GPS	4848					
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49XK9605	P8S	15	1 ROS 062796 0514 B0	03 59.64 N 130 00.42 E GPS	4709	29	4764	4749	36	1-6,9,10,12,23,24,26
49XK9605	P8S	15	1 ROS 062796 0803 EN	03 58.79 N 129 59.66 E GPS	4703					
49XK9605	P8S	16	1 ROS 062796 1055 BE	03 40.14 N 129 59.94 E GPS	3701					
49XK9605	P8S	16	1 ROS 062796 1155 B0	03 39.80 N 130 00.02 E GPS	3615	44	3698	3712	33	1-6
49XK9605	P8S	16	1 ROS 062796 1410 EN	03 38.74 N 130 00.39 E GPS	3949					
49XK9605	P8S	17	1 ROS 062796 1616 BE	03 20.07 N 129 59.96 E GPS	3910					
49XK9605	P8S	17	1 ROS 062796 1720 B0	03 19.72 N 130 00.31 E GPS	3886	40	3903	3900	36	1-6
49XK9605	P8S	17	1 ROS 062796 1956 EN	03 18.28 N 130 00.39 E GPS	3910					
49XK9605	P8S	18	1 ROS 062796 2204 BE	03 00.15 N 129 59.85 E GPS	3030					
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49XK9605	P8S	18	1 ROS 062896 0038 EN	02 59.28 N 130 00.21 E GPS	3118					
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49XK9605	P8S	19	1 ROS 062896 0329 B0	02 44.85 N 130 00.01 E GPS	3032		997	1000	36	1,2
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49XK9605	P8S	20	1 ROS 062896 1029 BE	02 30.07 N 130 00.02 E GPS	4015					
49XK9605	P8S	20	1 ROS 062896 1129 B0	02 29.84 N 130 00.17 E GPS	4023	15	4003	4048	36	1-6,9,10,12
49XK9605	P8S	20	1 ROS 062896 1325 EN	02 29.08 N 130 00.52 E GPS	4029					
49XK9605	P8S	21	1 ROS 062896 1714 BE	02 15.15 N 130 00.00 E GPS	4314					
49XK9605	P8S	21	1 ROS 062896 1831 B0	02 15.07 N 130 00.02 E GPS	4317	11	4295	4365	36	1-6
49XK9605	P8S	21	1 ROS 062896 2057 EN	02 14.58 N 129 59.84 E GPS	4307					
49XK9605	P8S	22	1 ROS 062896 2320 BE	01 59.93 N 129 59.94 E GPS	4402					
49XK9605	P8S	22	1 ROS 062996 0023 B0	01 59.61 N 130 00.29 E GPS	4396	14	4455	4452	36	1-6,9,10,12,23,24,26
49XK9605	P8S	22	1 ROS 062996 0232 EN	01 59.26 N 130 01.15 E GPS	4400					
49XK9605	P8S	23	1 ROS 062996 0850 BE	01 44.98 N 129 59.98 E GPS	3873					
49XK9605	P8S	23	1 ROS 062996 0951 B0	01 44.00 N 130 00.00 E GPS	3890	19	3857	3902	36	1-6
49XK9605	P8S	23	1 ROS 062996 1203 EN	01 44.79 N 130 01.08 E GPS	3947					
49XK9605	P8S	24	1 ROS 062996 1445 BE	01 30.09 N 129 59.91 E GPS	4131					
49XK9605	P8S	24	1 ROS 062996 1555 B0	01 29.71 N 130 00.17 E GPS	4113	10	4138	4174	36	1-6,9,10,12
49XK9605	P8S	24	1 ROS 062996 1826 EN	01 28.80 N 130 01.11 E GPS	4026					
49XK9605	P8S	25	1 ROS 062996 2145 BE	01 14.97 N 129 59.84 E GPS	3424					
49XK9605	P8S	25	1 ROS 062996 2251 B0	01 14.98 N 130 00.10 E GPS	3299	64	3343	3370	36	1-6
49XK9605	P8S	25	1 ROS 063096 0046 EN	01 15.05 N 130 00.73 E GPS	3225					
49XK9605	P8S	26	1 ROS 063096 0418 BE	00 59.96 N 129 59.51 E GPS	3020					
49XK9605	P8S	26	1 ROS 063096 0516 B0	01 00.14 N 129 59.81 E GPS	3022	9	3006	3033	36	1-6,9,10,12,23,24,26
49XK9605	P8S	26	1 ROS 063096 0715 EN	01 00.57 N 130 00.56 E GPS	3024					
49XK9605	P8S	27	1 ROS 063096 0950 BE	00 45.10 N 129 59.65 E GPS	1370					
49XK9605	P8S	27	1 ROS 063096 1024 B0	00 45.03 N 129 59.97 E GPS	1514	20	1451	1459	36	1-6
49XK9605	P8S	27	1 ROS 063096 1130 EN	00 45.00 N 130 00.45 E GPS	1562					